# **MEMO**



TO: 1495754 Ontario Ltd.

FROM: Aakash Bagchi, P.Eng., Saranya Jeyalakshmi

DATE: September 4, 2024

SUBJECT: Stormwater Management and Sanitary Servicing Study for 0 Esplanade Drive, Windsor,

ON

OUR FILE: 23-7174

## 1.0 Introduction

Dillon Consulting Limited (Dillon) has been retained by 1495754 Ontario Inc. to complete a stormwater management (SWM) and sanitary servicing study in support of the zoning by-law amendment for the proposed residential development located at 0 Esplanade Drive, in the City of Windsor (refer to Figure 1). The total site area is approximately 0.66 ha.



Figure 1: Location Map

#### Background Information

1.1

1.2

The following items were referred to while conducting the current analysis:

- Windsor-Essex Region Stormwater Management Standards Manual (ERCA, 2018) [WERSMSM];
- City of Windsor Development Manual (City of Windsor, 2015);
- Little River Watershed Flood Line Mapping -Final Hydraulic Report (Dillon, 2023);
- City of Windsor Sewer and Coastal Flooding Protection Master Plan (Dillon, 2020); and
- Stormwater Management Planning and Design Manual (MECP, 2003).

Stormwater runoff from the proposed development area will drain to an existing storm sewer maintenance hole (MH-7R9843) located within the limits of the proposed development. Sanitary flow from the site will drain to the sanitary sewer maintenance hole (MH-7S1380) located along Esplanade Drive. (Figure 1). The site plan for the proposed residential development of 0 Esplanade Drive is provided in Appendix A.

#### SWM Design Criteria

The criteria for SWM is to control flows from the proposed development to the estimated allowable release rate for all design storm event simulations, up to and including the 100-Year return event. In addition, the maximum depth of ponding on site during the governing 100-Year return period event simulation should not exceed 0.30 m above the lowest catch basin (CB) elevation.

The Climate Change stress test (approximately 40 % more volume and intensity than the 100-Year, 4-hour event) design storm event is to be simulated to assess the proposed SWM infrastructure's resiliency to adapt to the impacts of climate change.

The following design storm events, as recommended in the WERSMSM, were used to assess the on-site storage requirements under post-development conditions:

- 5-Year, 4-hour design storm using Chicago distribution with a 15-minute time interval and a total rainfall depth of 49.5 mm;
- 2-Year, 4-hour design storm using Chicago distribution with a 15-minute time interval and a total rainfall depth of 32 mm (Water Quality Storm);
- 100-Year, 4-hour design storm using Chicago distribution with a 15-minute time interval and a total rainfall depth of 81.6 mm to determine the required 100-Year design on-site storage; and
- Climate Change stress test, approximately 40 % more volume and intensity than the 100-Year 4hour event.

## 2.0 Existing Conditions

Under existing conditions, the site is vacant and covered in mostly grass. The topography of the current site is relatively flat and generally slopes towards Esplanade Drive to the south. Under existing conditions, considering current topography, some overland flow from the external parking lot area north of the existing site is expected to be routed through the proposed development area (refer to Figure 1). The site forms a part of the Little River watershed.

### 2.1 Soil Type

Based on the Essex Region Conservation Authority soil mapping, the soil within the site is mostly Brookston Clay which falls under the hydrologic soil group (HSG) classification of "D" soils that have high runoff potential.

#### 2.2 Existing Conditions Hydrologic Analysis

The existing site is 0.66 ha in area, currently undeveloped and mostly covered in grass. The existing condition hydrologic analysis was performed using the PCSWMM software. The proposed residential development area was modelled as one lumped subcatchment in PCSWMM. The allowable release rate for the 0.66 ha area has been estimated as 24.6 L/s. This corresponds to the peak runoff flow from the existing undeveloped site during the 5-Year design storm event simulation. To prevent any adverse impacts on the downstream system due to the increased imperviousness level in the proposed development area, the maximum stormwater flow rate from the site is expected to be maintained at or below the allowable release rate for all events up to and including the 100-Year event. The existing condition modelling parameters and results of the analysis are presented in Table 1.

Figure 1 shows the drainage area used for the existing conditions analysis to estimate allowable release rates for the development.

Table 1: Subcatchment Parameters and Release Rate

Catchment	Area (Ha)	Percent Impervious (%)	Other Subcatchment Parameters	Design Storm Event	Release Rate (L/s)
0 Esplanade Drive	0.66	0	Flow Length = 135 m Slope = 0.5 % Impervious Depression Storage = 2.5 mm Pervious Depression Storage = 7.5 mm Manning's N Impervious = 0.013 Manning's N Pervious = 0.24 Subarea Routing = Outlet (100%) Green-Ampt Infiltration Parameters: Suction Head = 180 mm Hydraulic Conductivity = 0.5 mm/hr Initial Deficit = 0.1	5-Year, 4-hour (Chicago)	24.6

## 3.0 Proposed Conditions Analysis

Under proposed conditions, the 0.66 ha multistoried residential development will consist of 8 one-bedroom units and 46 two-bedroom units. Runoff from the site is to be collected through CBs in the parking lot area and conveyed through a proposed storm sewer system in the development area to the existing storm sewer node MH-7R9843. Stormwater runoff storage is provided using a combination of surface and underground storage to restrict flows to the estimated allowable release rate.

The proposed residential development area was modelled as one lumped subcatchment in PCSWMM. The modelling schematic is shown in Figure 2.

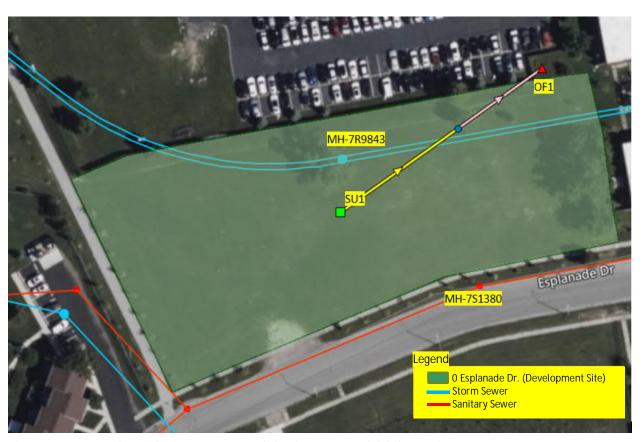


Figure 2: Proposed Development Area and the SWMM Model Schematic

The storage node (SU1) in the model represents surface storage around CB locations in the parking lot as well as sub-surface storage. The parameters used to set up the proposed conditions PCSWMM model are summarized in Table 2. The soil types are composed of Brookston Clay which has a hydrologic soil group (HSG) D classification. Green-Ampt infiltration method was used for SWMM hydrologic calculations. Dynamic wave routing method was applied for hydraulic conveyance in the model.

Table 2: Subcatchment Parameters and Release Rate

Catchment	Area (Ha)	Percent Impervious (%)	Other Subcatchment Parameters
0 Esplanade Drive	0.66	90	Flow Length = 77 m Slope = 1 % Impervious Depression Storage = 2.5 mm Pervious Depression Storage = 7.5 mm Manning's N Impervious = 0.013 Manning's N Pervious = 0.24 Subarea Routing = Outlet (100%) Green-Ampt Infiltration Parameters: Suction Head = 180 mm Hydraulic Conductivity = 0.5 mm/hr Initial Deficit = 0.1

The release rate from the site is maintained at or below the estimated allowable release rate using an orifice of size 0.1 m diameter. A flap valve is proposed along with the orifice to prevent any backwater flow from the downstream municipal sewer system.

Boundary condition restrictions were applied to the model outfall (OF1), representing the MH-7R9843 location. This is to simulate the existing tailwater conditions in the downstream municipal sewer system. The head time series for the node MH-7R9843 were provided by the City from the City-wide dynamic sewer model developed through the Sewer and Coastal Flood Protection Master Plan (SMP). The head time series are represented in Appendix B.

The PCSWMM input and output files for existing and proposed conditions models are included in Appendix C.

## 3.1 Stormwater Quantity Control

Based on the pre-development allowable release rate of 24.6 L/s, the required volume under 100-Year, 4-hour (Chicago distribution) design storm event has been estimated to be 404 m<sup>3</sup>. The proposed conditions model results are summarized in Table 3.

Table 3: Proposed Conditions Model Results

Design Storm Events		Storage on Site							
	Peak Flow Rate (L/s)	Total Volume (m³)	Parking lot Storage (m³)	Underground Storage (m³)	Max. depth of surface storage at CB locations (m)				
Water Quality Test	14.5	105	0	105	0				
5-Year, 4-hour (Chicago)	23.9	183	0	183	0				
100-Year, 4-hour (Chicago)	14.5	404	221	183	0.22				
Climate Change Stress Test	15.0	586	403	183	> 0.30				

A combination of surface and underground storage was provided to restrict flows to the estimated allowable release rate in the residential development.

It is noted that the release from the site during the 5-Year event is estimated to be higher than the less frequent design storm events evaluated. The head time-series provided by the City for the analysis show a lower maximum Hydraulic Grade Line (HGL) (175.70 m) during the 5-Year event, compared to maximum HGL during the 100-Year event (177.97 m). The higher HGL at the outfall leads to lower release rate and more on-site storage during the larger rainfall events.

## 3.2 Impacts of Climate Change

During the Climate Change stress test simulation, the maximum depth of stormwater storage around CB locations is expected to be greater than 0.3 m. This is expected because the climate change event has approximately 40% more volume and intensity compared to the 100-Year 4-hour event. For events more severe than 100-Year, 4-hour event, an overland flow route will be provided from the site towards Little River.

#### 3.3 External Drainage Area

Under existing conditions, some overland flow from the external parking lot area located north of the proposed development area (refer to Figure 1) is expected to be routed through the proposed development area. Under proposed conditions, this flow will need to be accounted in on-site storage calculations, or an alternate overland flow route to Little River will need to be provided. This will be further designed during the detailed design stage.

#### 3.4 Stormwater Quality Control

Since the impervious area on the site is increasing as compared to existing conditions, measures are proposed to be undertaken to treat the quality of the stormwater runoff being discharged into the municipal storm sewers, and ultimately to Little River. Stormwater quality treatment will be provided using an oil-grit separator (OGS) positioned upstream of the existing municipal storm sewer outlet at MH-7R9843.

The 1200 mm diameter, Hydro International First Defense (FD-4HC) unit supplied by ADS, or an approved equivalent, is recommended for this application. The OGS unit is designed to meet the Ministry of Environment, Conservation and Parks (MECP) design requirements for 70% TSS removal (normal level of protection), for an upstream drainage area of 0.66 ha. Sizing details for the Water Quality Unit (WQU) recommended for the proposed development, provided by the supplier, are included in Appendix D.

#### 3.5 Erosion and Sediment Control During Construction

Erosion and sediment control measures are to be implemented during construction in accordance with the "Guidelines on Erosion and Sediment Control for Urban Construction Sites" (Government of Ontario, May 1987) and "Construction Specification for Temporary Erosion and Sediment Control Measures" (OPSS 805).

## 4.0 Sanitary Servicing Under Proposed Conditions

Under the proposed conditions, the sanitary flow from the residential development will be discharged to the existing sanitary sewer (MH-7S1380) located on Esplanade Drive, in proximity of the site (refer to Figure 2). The ultimate flow under the proposed conditions was estimated based on the parameters listed in Table 4, and the flow calculation has been summarized in Table 5.

Table 4: Proposed Conditions Sanitary Flow Parameters

Parameter	Value
Residential – Population	1.5 people/one-bedroom unit; 2.5 people/two-bedroom unit <sup>1</sup>
Residential Sewage Flow Rate	0.0042 L/person-capita <sup>2</sup>
Peak Flow Factor	6 (six) <sup>2</sup>
Infiltration	1 L/s/ha³

<sup>&</sup>lt;sup>1</sup> Based on recent communication from the City of Windsor

Table 5: Ultimate Sanitary Flow Calculation

Residential Sewage Flow (L/s/capita)	Ultimate	Peak Flow	Total Wastewater Flow (L/s)	Inflow ar	Ultimate Sanitary		
	Population <sup>1</sup>	Factor		Site Area (ha)	Rate (L/s/ha)	Flow (L/s)	Flow <sup>2</sup> (L/s)
0.0042	127	6	3.20	0.66	1.0	0.66	3.86

<sup>&</sup>lt;sup>1</sup> 8 one-bedroom units and 46 two-bedroom units

The ultimate sanitary flow is estimated to be 3.86 L/s and will be discharged to the existing sanitary sewer (MH-7S1380).

#### 4.1 Measures to prevent Inflow and Infiltration (I&I) into the sanitary sewer system

Placement of sanitary manhole lids/seals outside of the on-site 100-Year surface ponding extents is recommended to limit possible I&I. More details will be provided in the detailed design stage.

<sup>&</sup>lt;sup>2</sup> Based on City of Windsor Development Manual, 2015

<sup>&</sup>lt;sup>3</sup> Based on City's Sewer and Coastal Flooding Protection Master Plan (Dillon, 2020)

<sup>&</sup>lt;sup>2</sup> Based on Section 9.1.2-City of Windsor Development Manual, 2015

# 5.0 Flood Proofing

According to the WERSMSM design requirements, the minimum lowest building opening elevation should be the higher of the following:

- 0.30 m above the regulatory flood level for a neighboring watercourse;
- 0.30 m above the 100-Year water surface elevation (WSEL) on-site; or
- Climate Change stress test WSEL on-site.

The 100-year water level in Little River at the nearest point to the site (upstream of Tecumseh road crossing), based on pre-consultation with ERCA (refer to Appendix E) is 178.14 m. Therefore, the minimum building opening will be 178.44 m, or 0.30 m above 100-Year WSEL on-site, or Climate Change stress test WSEL on-site, whichever is greater.

The WSEL on-site for the 100-Year and Climate Change stress test design storm events will be evaluated after detailed grading design for the site is completed at a future date. No additional stormwater related requirements are necessary at this time.

## **Summary and Conclusions**

6.0

Based on the SWM analysis completed for the proposed development site, the following conclusions were drawn.

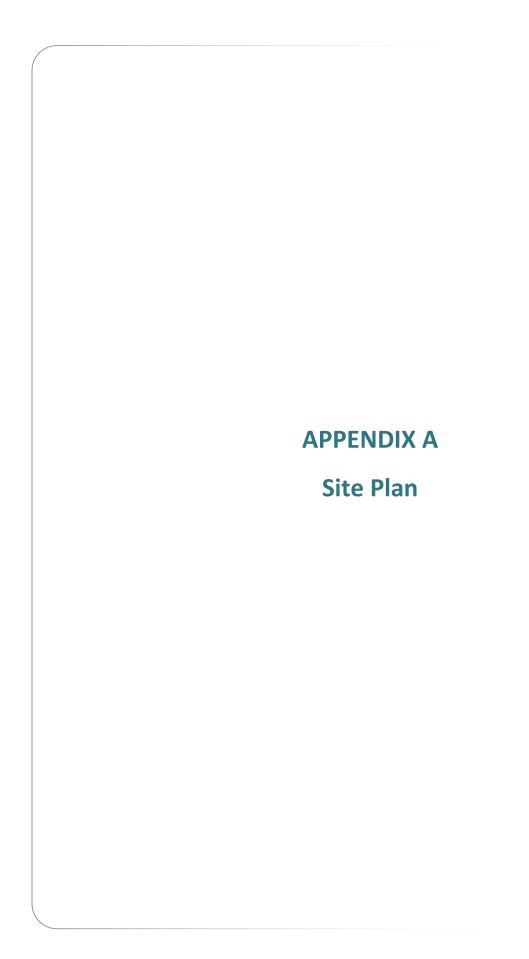
- The maximum allowable release rate under pre-existing condition from the site is 24.6 L/s. The peak discharge from the proposed development will be restricted to this value for all events up to and including the 100-Year return period rainfall event.
- It has been demonstrated through a modelling analysis that the peak outflow from the site during all proposed conditions simulations, including the Climate Change stress test simulation, was less than the allowable release rate.
- Impact of tailwater conditions due to surcharge conditions in the downstream municipal sewer system have been accounted for in the dynamic modelling analysis.
- The flow rate under proposed development conditions has been maintained at or below the allowable release rate for all events up to and including the 100-Year return period rainfall event using an orifice of size 0.1 m diameter.
- Along with the orifice, a flap valve is recommended at the site outlet to prevent backwater flow from the downstream municipal storm sewer system. The flap valve will protect the proposed underground storage system against any high water level conditions in the Little River Drain.
- Stormwater runoff storage on site was provided using surface ponding around CB locations in the parking lot area and using an underground storage system.
- During the 100-Year, 4-hour (Chicago) proposed conditions simulation, total on-site storage estimated was approximately 404 m<sup>3</sup>.
- Stormwater quality control will be provided on site using an OGS unit, providing 70% TSS removal. The 1200 mm diameter FD-4HC unit, supplied by ADS, or an approved equivalent, is recommended.
- Total sanitary discharge from the site is estimated to be 3.86 L/s. This includes wastewater flows generated from the residential development as well as an allowance for Inflow and Infiltration. Sanitary flows will be discharged to the existing sanitary sewer (node MH-7S1380) located on Esplanade Drive. Placement of sanitary manhole lids/seals outside of the on-site 100-year ponding extents is recommended to limit the possible I&I.

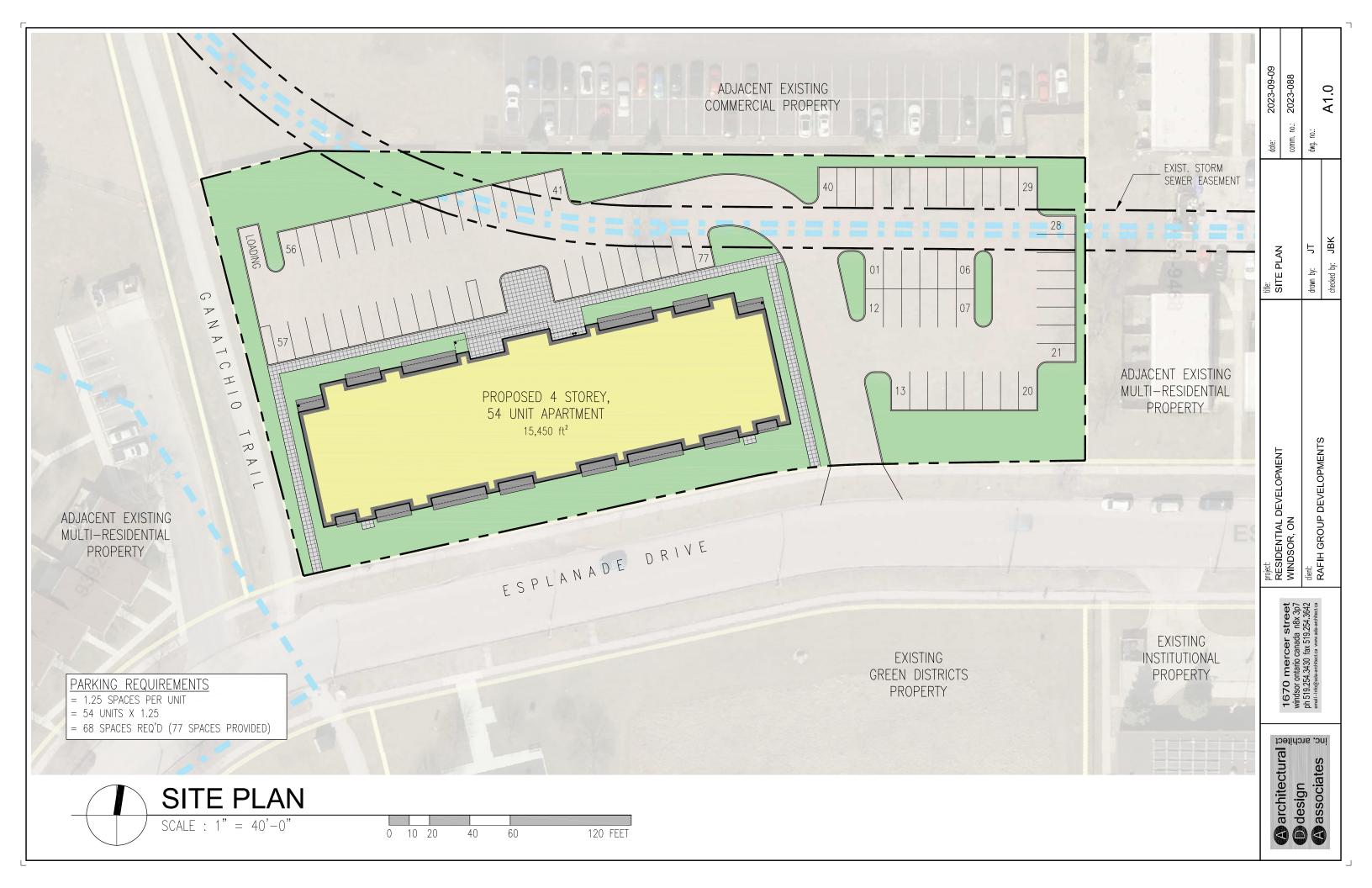
We trust that our findings provide you with the information that you require at this time. We would be pleased to meet with you to review our findings in further detail. If you have any questions in the interim, please feel free to contact the undersigned.

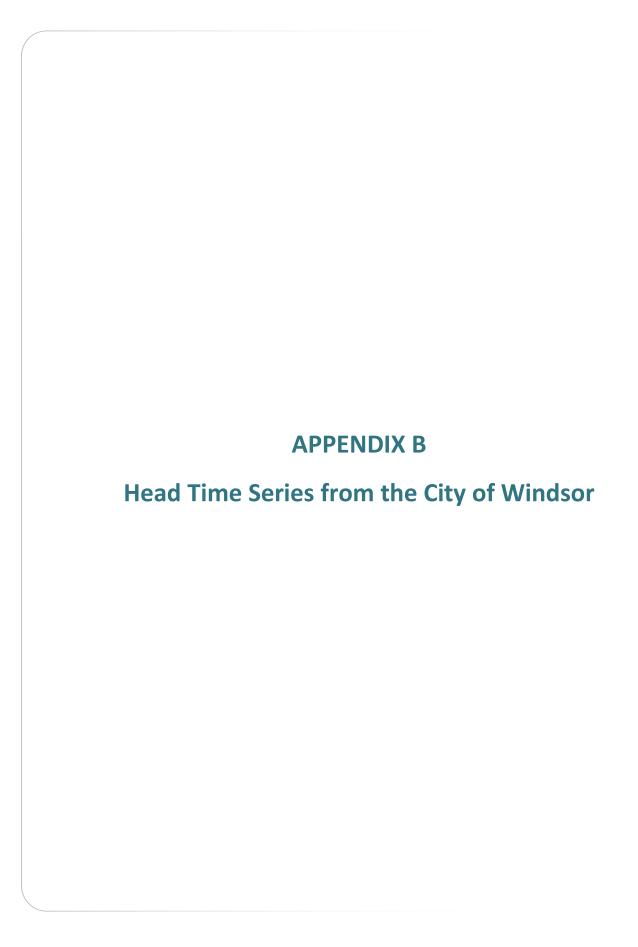
Sincerely,

#### **DILLON CONSULTING LIMITED**

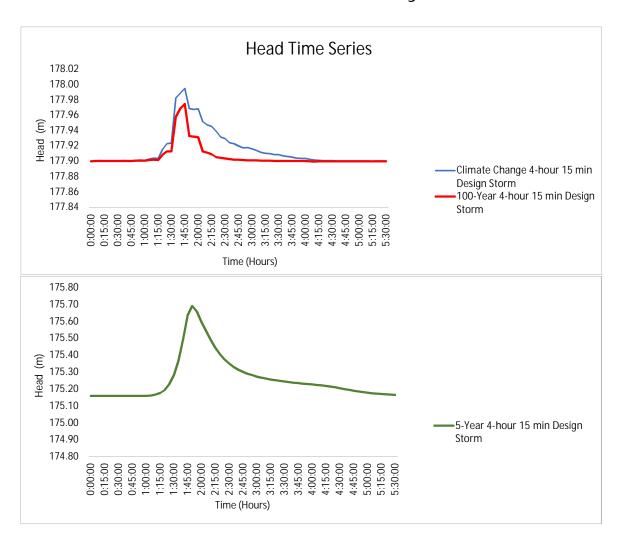
Aakash Bagchi, P.Eng. Water Resources Engineer Saranya Jeyalakshmi, Ph.D, Water Resources Designer

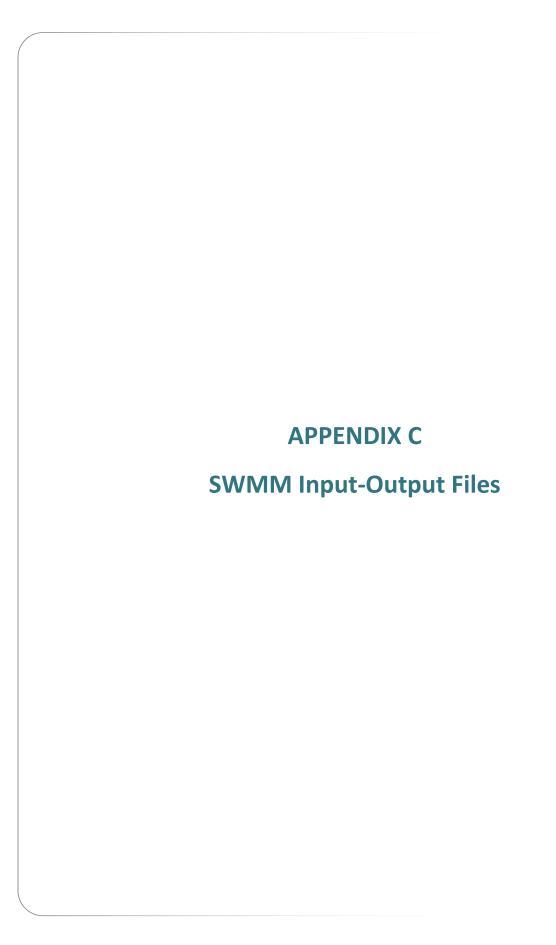






## Head Time Series from the City of Windsor





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# Existing 5-Year Output

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Number of rain gag Number of subcatch Number of nodes Number of links Number of pollutan Number of land use	ments 1 1 0 ts 0					
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Raingage Summary						
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Raingage	5Year4hour15min		INTENSIT	Y 15 mir	 1.	
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Name	Area W 	idth %Imperv	 \ &2TOE	e Rain Gag	je 	Outlet 
S1	0.66 4	8.89 0.00	0.500	0 Raingage	2	OF1
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Node Summary *******						
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Analysis Options						
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Infiltration Method Surcharge Method . Starting Date	d HORTON					

Antecedent Dry Days	0.0
Report Time Step	00:01:00
Wet Time Step	00:05:00
Dry Time Step	00:05:00

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Total Precipitation  Evaporation Loss  Infiltration Loss  Surface Runoff  Final Storage  Continuity Error (%)	0.033 0.000 0.015 0.017 0.000 -0.091	49.475 0.000 23.269 26.251 0.000
**************************************	Volume hectare-m	Volume 10^6 ltr
Dry Weather Inflow  Wet Weather Inflow  Groundwater Inflow	0.000 0.017 0.000	0.000 0.173 0.000
RDII Inflow  External Inflow  External Outflow	0.000 0.000 0.017	0.000 0.000 0.173
Flooding Loss  Evaporation Loss  Exfiltration Loss	0.000 0.000 0.000	0.000 0.000 0.000
Initial Stored Volume Final Stored Volume Continuity Error (%)	0.000 0.000 0.000	0.000

Subcatchment	Total Precip mm	Total Runon mm	Total Evap mm	Total Infil mm	Imperv Runoff mm	Perv Runoff mm	Total Runoff mm	Total Runoff 10^6 ltr	Peak Runoff CMS	Runoff Coeff
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; R1_1	0.5	0.5	0	NO	0						
CURVES]	Туре	X-Value	Y-Value								
; Parkinglot Parkinglot Parkinglot Parkinglot Parkinglot	Storage	0 1.49 1.5 2.9	122 122 0.7 0.7 2681								
parkingonly parkingonly parkingonly	Storage	0 2.9 3.2	0.7 0.7 2681								

[TIMESERIES]		

;;Name	Date	Time	Value
100year4hour15		0:00	3.95
100year4hour15	Smin	0:15	4.87
100year4hour15	Smin	0:30	6.36
100year4hour15	Smin	0:45	9.19
100year4hour15	Smin	1:00	16.45
100year4hour15	Smin	1:15	46.45
100year4hour15	Smin	1:30	143.67
100year4hour15	min	1:45	32.45
100year4hour15	min	2:00	17.25
100year4hour15	min	2:15	11.53
100year4hour15	min	2:30	8.62
100year4hour15	min	2:45	6.87
100year4hour15	Smin	3:00	5.71
100year4hour15	Smin	3:15	4.89
100year4hour15	Smin	3:30	4.28
100year4hour15	Smin	3:45	3.81
100year4hour15	Smin	4:00	0
100yearTW		0:00:00	177.900009
100yearTW		0:05:00	177.900299
100yearTW		0:10:00	177.900497
100yearTW		0:15:00	177.900375
100yearTW		0:20:00	177.900269
100yearTW		0:25:00	177.900284
100yearTW		0:30:00	177.900299
100yearTW		0:35:00	177.900421
100yearTW		0:40:00	177.900452
100yearTW		0:45:00	177.900360
100yearTW		0:50:00	177.900696
100yearTW		0:55:00	177.900879
100yearTW		1:00:00	177.900696
100yearTW		1:05:00	177.901749
100yearTW		1:10:00	177.902328
100yearTW		1:15:00	177.901932
100yearTW		1:20:00	177.908966
100yearTW		1:25:00	177.913147
100yearTW		1:30:00	177.912811
100yearTW		1:35:00	177.958206
100yearTW		1:40:00	177.968964
100yearTW		1:45:00	177.974808
100yearTW		1:50:00	177.933060
100yearTW		1:55:00	177.932068
100yearTW		2:00:00	177.931396
100yearTW		2:05:00	177.913055
100yearTW		2:10:00	177.911118
100yearTW		2:15:00	177.909088
100yearTW		2:20:00	177.905502
100yearTW		2:25:00	177.904617
100yearTW		2:30:00	177.903885
100yearTW		2:35:00	177.902771
100yearTW		2:40:00	177.902191
100yearTW		2:45:00	177.902130
100yearTW		2:50:00	177.901672
100yearTW		2:55:00	177.901382

100yearTW	3:00:00	177.901337
100yearTW	3:05:00	177.901108
100yearTW	3:10:00	177.900925
100yearTW	3:15:00	177.900909
100yearTW	3:20:00	177.900757
100yearTW	3:25:00	177.900635
100yearTW	3:30:00	177.900635
100yearTW	3:35:00	177.900543
100yearTW	3:40:00	177.900467
100yearTW	3:45:00	177.900467
100yearTW	3:50:00	177.900391
100yearTW	3:55:00	177.900345
100yearTW	4:00:00	177.900345
100yearTW	4:05:00	177.899887
100yearTW	4:10:00	177.899750
100yearTW	4:15:00	177.899918
100yearTW	4:20:00	177.900177
100yearTW	4:25:00	177.900040
100yearTW	4:30:00	177.899872
100yearTW	4:35:00	177.899963
100yearTW	4:40:00	177.900085
100yearTW	4:45:00	177.900101
100yearTW	4:50:00	177.899979
100yearTW	4:55:00	177.899948
100yearTW	5:00:00	177.900024
100yearTW	5:05:00	177.900116
100yearTW	5:10:00	177.900024
100yearTW	5:15:00	177.899963
100yearTW	5:20:00	177.900009
100yearTW	5:25:00	177.900070
100yearTW	5:30:00	177.900040
5Year4hour15min	0:00	2.58
5Year4hour15min	0:15	3.13
5Year4hour15min	0:30	4.02
5Year4hour15min	0:45	5.66
5Year4hour15min	1:00	9.76
5Year4hour15min	1:15	26.72
5Year4hour15min	1:30	88.4
5Year4hour15min	1:45	18.73
5Year4hour15min	2:00	10.21
5Year4hour15min	2:15	6.99
5Year4hour15min	2:30	5.33
5Year4hour15min	2:45	4.31
5Year4hour15min	3:00	3.64
5Year4hour15min	3:15	3.15
5Year4hour15min	3:30	2.78
5Year4hour15min	3:45	2.49
5Year4hour15min	4:00	0
5yearTW	0:00:00	175.16
5yearTW	0:05:00	175.16
5yearTW	0:10:00	175.16
5yearTW	0:15:00	175.16
5yearTW	0:20:00	175.16
5yearTW	0:25:00	175.16
5yearTW	0:30:00	175.16
-		

5yearTW	0:35:00	175.16
5yearTW	0:40:00	175.16
5yearTW	0:45:00	175.16
5yearTW	0:50:00	175.16
5yearTW	0:55:00	175.16
5yearTW	1:00:00	175.16
5yearTW	1:05:00	175.16
5yearTW	1:10:00	175.17
5yearTW	1:15:00	175.18
5yearTW	1:20:00	175.19
5yearTW	1:25:00	175.23
5yearTW	1:30:00	175.28
5yearTW	1:35:00	175.37
5yearTW	1:40:00	175.50
5yearTW	1:45:00	175.64
5yearTW	1:50:00	175.69
5yearTW	1:55:00	175.66
5yearTW	2:00:00	175.60
5yearTW	2:05:00	175.54
5yearTW	2:10:00	175.49
5yearTW	2:15:00	175.44
5yearTW	2:20:00	175.41
5yearTW	2:25:00	175.38
5yearTW	2:30:00	175.35
5yearTW	2:35:00	175.33
5yearTW	2:40:00	175.31
5yearTW	2:45:00	175.31
5yearTW	2:50:00	175.29
5yearTW	2:55:00	175.28
5yearTW	3:00:00	175.27
5yearTW	3:05:00	175.27
5yearTW	3:10:00	175.26
5yearTW	3:15:00	175.26
5yearTW	3:20:00	175.25
5yearTW	3:25:00	175.25
5yearTW	3:30:00	175.24
5yearTW	3:35:00	175.24
5yearTW	3:40:00	175.24
5yearTW	3:45:00	175.24
5yearTW	3:50:00	175.23
5yearTW	3:55:00	175.23
5yearTW	4:00:00	175.23
5yearTW	4:05:00	175.23
5yearTW	4:10:00	175.22
_		
5yearTW	4:15:00	175.22
5yearTW	4:20:00 4:25:00	175.21
5yearTW	4:30:00	175.21 175.21
5yearTW	4:35:00	
5yearTW		175.20
5yearTW	4:40:00	175.19
5yearTW	4:45:00	175.19
5yearTW	4:50:00	175.19
5yearTW	4:55:00	175.18
5yearTW	5:00:00	175.18
5yearTW	5:05:00	175.18
5yearTW	5:10:00	175.17
5yearTW	5:15:00	175.17

5yearTW	5:20:00	175.17
5yearTW	5:25:00	175.17
5yearTW	5:30:00	175.17
ClimateChangeTW	0:00:00	177.90
ClimateChangeTW	0:05:00	177.90
ClimateChangeTW	0:10:00	177.90
ClimateChangeTW	0:15:00	177.90
ClimateChangeTW	0:20:00	177.90
ClimateChangeTW	0:25:00	177.90
ClimateChangeTW	0:30:00	177.90
ClimateChangeTW	0:35:00	177.90
ClimateChangeTW	0:40:00	177.90
ClimateChangeTW	0:45:00	177.90
ClimateChangeTW	0:50:00	177.90
ClimateChangeTW	0:55:00	177.90
ClimateChangeTW	1:00:00	177.90
ClimateChangeTW	1:05:00	177.90
ClimateChangeTW	1:10:00	177.90
ClimateChangeTW	1:15:00	177.90
ClimateChangeTW	1:20:00	177.92
ClimateChangeTW	1:25:00	177.92
ClimateChangeTW	1:30:00	177.92
ClimateChangeTW	1:35:00	177.98
ClimateChangeTW	1:40:00	177.99
ClimateChangeTW	1:45:00	178.00
ClimateChangeTW	1:50:00	177.97
ClimateChangeTW	1:55:00	177.97
ClimateChangeTW	2:00:00	177.97
ClimateChangeTW	2:05:00	177.95
ClimateChangeTW	2:10:00	177.95
ClimateChangeTW	2:15:00	177.95
ClimateChangeTW	2:20:00	177.94
ClimateChangeTW	2:25:00 2:30:00	177.93 177.93
ClimateChangeTW	2:35:00	177.93
ClimateChangeTW ClimateChangeTW	2:40:00	177.92
ClimateChangeTW	2:45:00	177.92
ClimateChangeTW	2:43:00	177.92
ClimateChangeTW	2:55:00	177.92
ClimateChangeTW	3:00:00	177.92
ClimateChangeTW	3:05:00	177.91
ClimateChangeTW	3:10:00	177.91
ClimateChangeTW	3:15:00	177.91
ClimateChangeTW	3:20:00	177.91
ClimateChangeTW	3:25:00	177.91
ClimateChangeTW	3:30:00	177.91
ClimateChangeTW	3:35:00	177.91
ClimateChangeTW	3:40:00	177.91
ClimateChangeTW	3:45:00	177.91
ClimateChangeTW	3:50:00	177.90
ClimateChangeTW	3:55:00	177.90
ClimateChangeTW	4:00:00	177.90
ClimateChangeTW	4:05:00	177.90
ClimateChangeTW	4:10:00	177.90
ClimateChangeTW	4:15:00	177.90
ClimateChangeTW	4:20:00	177.90
<b>.</b>		

ClimateChangeTW	4:25:00	177.90		
ClimateChangeTW	4:30:00	177.90		
ClimateChangeTW	4:35:00	177.90		
ClimateChangeTW	4:40:00	177.90		
ClimateChangeTW	4:45:00	177.90		
ClimateChangeTW	4:50:00	177.90		
ClimateChangeTW	4:55:00	177.90		
ClimateChangeTW	5:00:00	177.90		
ClimateChangeTW	5:05:00	177.90		
ClimateChangeTW	5:10:00	177.90		
ClimateChangeTW	5:15:00	177.90		
ClimateChangeTW	5:20:00	177.90		
ClimateChangeTW	5:25:00	177.90		
ClimateChangeTW	5:30:00	177.90		
[REPORT]				
;;Reporting Opti	ons.			
INPUT YES				
CONTROLS NO				
SUBCATCHMENTS AL	ıL			
NODES ALL				
LINKS ALL				
[TAGS]				
[MAP]				
DIMENSIONS	341299.87365 4	686121.25085	341460.28335	4686224.14815
UNITS	Meters			
[COORDINATES]				
=	X-Coord	V-Coord		
		4686194.004		
		4686209.471		
SU1	341379.002	4686172.379		
[VERTICES]				
;;Link	X-Coord	Y-Coord		
;;				
[ DOI MOOMU ]				
[POLYGONS]	Y-Coord	V-Coord		
;;Subcatchment		Y-Coord		
;;Subcatchment;;				
;;Subcatchment ;; S1	341322.26	4686188.935		
;;Subcatchment ;;S1 S1	341322.26 341340.95	4686188.935 4686192.156		
;;Subcatchment ;;S1 S1 S1	341322.26 341340.95 341385.988	4686188.935 4686192.156 4686199.087		
<pre>;;Subcatchment ;; S1 S1 S1 S1</pre>	341322.26 341340.95 341385.988 341431.872	4686188.935 4686192.156 4686199.087 4686206.661		
<pre>;;Subcatchment ;; S1 S1 S1 S1 S1 S1</pre>	341322.26 341340.95 341385.988 341431.872 341445.869	4686188.935 4686192.156 4686199.087 4686206.661 4686208.166		
<pre>;;Subcatchment ;; S1 S1 S1 S1 S1 S1 S1 S1</pre>	341322.26 341340.95 341385.988 341431.872 341445.869 341447.582	4686188.935 4686192.156 4686199.087 4686206.661 4686208.166 4686199.491		
<pre>;;Subcatchment ;; S1 S1 S1 S1 S1 S1 S1 S1</pre>	341322.26 341340.95 341385.988 341431.872 341445.869 341447.582 341449.205	4686188.935 4686192.156 4686199.087 4686206.661 4686208.166 4686199.491 4686192.561		
<pre>;;Subcatchment ;; S1 S1 S1 S1 S1 S1 S1 S1 S1</pre>	341322.26 341340.95 341385.988 341431.872 341445.869 341447.582 341449.205 341451.691	4686188.935 4686192.156 4686199.087 4686206.661 4686208.166 4686199.491 4686192.561 4686171.599		
<pre>;;Subcatchment ;; S1 S1</pre>	341322.26 341340.95 341385.988 341431.872 341445.869 341447.582 341449.205 341451.691 341452.992	4686188.935 4686192.156 4686199.087 4686206.661 4686208.166 4686199.491 4686192.561 4686171.599 4686162.957		
<pre>;;Subcatchment ;; S1 S1</pre>	341322.26 341340.95 341385.988 341431.872 341445.869 341447.582 341449.205 341451.691 341452.992 341406.432	4686188.935 4686192.156 4686199.087 4686206.661 4686208.166 4686199.491 4686192.561 4686171.599 4686162.957 4686154.901		
<pre>;;Subcatchment ;; S1 S1</pre>	341322.26 341340.95 341385.988 341431.872 341445.869 341447.582 341449.205 341451.691 341452.992 341406.432 341332.802	4686188.935 4686192.156 4686199.087 4686206.661 4686208.166 4686199.491 4686192.561 4686171.599 4686162.957 4686154.901 4686125.928		
<pre>;;Subcatchment ;; S1 S1</pre>	341322.26 341340.95 341385.988 341431.872 341445.869 341447.582 341449.205 341451.691 341452.992 341406.432 341332.802	4686188.935 4686192.156 4686199.087 4686206.661 4686208.166 4686199.491 4686192.561 4686171.599 4686162.957 4686154.901		

Y-Coord

;;Storage Node X-Coord

## Proposed Conditions 5-Year 4-hour Output Files

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.2 (Build 5.2.4) \*\*\*\*\* Element Count \*\*\*\*\* Number of rain gages ..... 1 Number of subcatchments ... 1 Number of nodes ..... 3 Number of links ..... 2 Number of pollutants ..... 0 Number of land uses ..... 0 \*\*\*\*\* Raingage Summary \*\*\*\*\* Data Recording Name Data Source Type Interval 5Year4hour15min INTENSITY 15 min. Raingage \*\*\*\*\* Subcatchment Summary \*\*\*\*\*\* Name Width %Imperv Outlet Area %Slope Rain Gage \_\_\_\_\_ S1 90.00 1.0000 Raingage \*\*\*\*\* Node Summary \*\*\*\*\* Invert Max. Ponded External Name Elev. Depth Inflow Type J1 JUNCTION 175.60 3.50 0.0 OF1 OUTFALL 175.10 0.00 0.0 SU1 STORAGE 175.90 3.20 0.0 \*\*\*\*\* Link Summary \*\*\*\*\* From Node Length %Slope Roughness Type OR1\_1 SU1 J1 CONDUIT 10.0 3.0014 0.0130 OR1\_2 J1 OF1 ORIFICE \*\*\*\*\*\* Cross Section Summary \*\*\*\*\*\*

Full

Full

Hyd.

Max. No. of

Full

Conduit	Shape	Depth	Area	Rad.	Width	Barrels	Flow
OR1 1	CIRCULAR	0.30	0.07	0.07	0.30	1	0.17

#### \* \* \* \* \* \* \* \* \* \* \* \* \* \* \* \*

#### Analysis Options \*\*\*\*\*

Flow Units ..... CMS

Process Models:

Rainfall/Runoff ..... YES RDII ..... NO Snowmelt ..... NO Groundwater ..... NO Flow Routing ..... YES Ponding Allowed ..... YES Water Quality ..... NO Infiltration Method ..... HORTON Flow Routing Method ..... DYNWAVE Surcharge Method ..... EXTRAN Starting Date ..... 04/29/2024 00:00:00 Ending Date ...... 04/30/2024 00:00:00 Antecedent Dry Days ..... 0.0

Report Time Step ...... 00:01:00 Wet Time Step ...... 00:05:00 Dry Time Step ...... 00:05:00 Routing Time Step ..... 0.50 sec Variable Time Step ..... YES

Maximum Trials ..... 8 Number of Threads ..... 1

Head Tolerance ..... 0.001500 m

*****	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
* * * * * * * * * * * * * * * * * * * *		
Total Precipitation	0.033	49.475
Evaporation Loss	0.000	0.000
Infiltration Loss	0.001	1.751
Surface Runoff	0.030	45.790
Final Storage	0.001	2.252
Continuity Error (%)	-0.642	
******	Volume	Volume
Flow Routing Continuity	hectare-m	10 <b>^</b> 6 ltr
******		
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.030	0.302
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	0.030	0.302
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000

Final Stored Volume ..... 0.000 0.000 Continuity Error (%) ..... 0.000

All links are stable.

Convergence obtained at all time steps.

Minimum Time Step 0.50 sec 0.50 sec Average Time Step Maximum Time Step 0.50 sec % of Time in Steady State : Average Iterations per Step: 2.00 % of Steps Not Converging : 0.00 Time Step Frequencies 0.500 - 0.500 sec : 100.00 % 0.500 - 0.500 sec 0.00 %

Total Total Peak Runoff Total Total Imperv Perv Total Total Precip Runon Evap Infil Runoff Runoff Runoff Runoff Coeff Runoff Subcatchment 10^6 ltr CMS mm mm mm mm mm mm mm \_\_\_\_\_\_ 49.48 0.00 42.54 45.79 0.30 0.16 0.926

-----

		Depth	Depth	HGL	0ccu	rrence	Max Depth
Node	Type	Meters	Meters	Meters	days	hr:min	Meters
J1	JUNCTION	0.29	3.09	178.69	0	02:07	3.09
OF1	OUTFALL	0.09	0.59	175.69	0	01:50	0.59
SU1	STORAGE	0.21	2.80	178.70	0	02:07	2.80

\_\_\_\_\_\_ Lateral Total Maximum Maximum Lateral Total Time of Max Inflow Inflow Balance Inflow Inflow Occurrence Volume Volume Error Node Type CMS CMS days hr:min 10^6 ltr 10^6 ltr Percent \_\_\_\_\_\_ JUNCTION 0.000 0.024 0 02:07 0 0.302 -0.002 J1 0.000 0.024 0 02:07 0 0.302 0.000 OF1 OUTFALL SU1 STORAGE 0.160 0.160 0 01:45 0.302 0.302 -0.000

Surcharging occurs when water rises above the top of the highest conduit.

Max. Height Min. Depth

			max. Height	Min. Depth
		Hours	Above Crown	Below Rim
Node	Type	Surcharged	Meters	Meters
J1	JUNCTION	5.90	2.790	0.410

No nodes were flooded.

Average Avg Evap Exfil Maximum Max Time of Max Maximum
Volume Pcnt Pcnt Pcnt Volume Pcnt Occurrence Outflow
Storage Unit 1000 m³ Full Loss Loss 1000 m³ Full days hr:min CMS

SU1 0.024 4.1 0.0 0.0 0.183 31.3 0 02:07 0.024

 \*\*\*\*\*

	Flow	Avg	Max	Total
	Freq	Flow	Flow	Volume
Outfall Node	Pcnt	CMS	CMS	10 <b>^</b> 6 ltr
OF1	41.09	0.009	0.024	0.302
System	41.09	0.009	0.024	0.302

Link	Type	1 1	Time of Max Occurrence days hr:min	Maximum  Veloc  m/sec	Max/ Full Flow	Max/ Full Depth
OR1_1 OR1_2	CONDUIT ORIFICE	0.024 0.024	0 02:07 0 02:07	0.40	0.14	1.00

	 Adjusted			Fract	ion of	Time	in Flo	w Clas	s	
Conduit	/Actual Length	Dry	Up Dry		Sub Crit	_	_			Inlet Ctrl
OR1 1	1.00	0.03	0.00	0.00	0.71	0.26	0.00	0.00	0.72	0.00

				Hours	Hours
		Hours Full		Above Full	Capacity
Conduit	Both Ends	Upstream	Dnstream	Normal Flow	Limited
OR1_1	4.52	4.52	5.90	0.01	0.01

Analysis begun on: Wed May 8 12:22:18 2024 Analysis ended on: Wed May 8 12:22:18 2024

Total elapsed time: < 1 sec

## Proposed Conditions 100-Year 4-hour Output Files

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.2 (Build 5.2.4) \*\*\*\*\* Element Count \*\*\*\*\* Number of rain gages ..... 1 Number of subcatchments ... 1 Number of nodes ..... 3 Number of links ..... 2 Number of pollutants ..... 0 Number of land uses ..... 0 \*\*\*\*\* Raingage Summary \*\*\*\*\* Data Recording Name Data Source Type Interval 100year4hour15min INTENSITY 15 min. Raingage \*\*\*\*\*\* Subcatchment Summary \*\*\*\*\*\* Name Width Outlet %Imperv %Slope Rain Gage Area -----S1 0.66 90.00 1.0000 Raingage \*\*\*\*\* Node Summary \*\*\*\*\*\* Invert Max. Ponded External Name Elev. Depth Inflow Type 175.60 J1 JUNCTION 3.50 0.0 OF1 175.10 0.00 0.0 OUTFALL SU1 STORAGE 175.90 3.20 0.0 \*\*\*\*\* Link Summary \*\*\*\*\*\* From Node To Node Length %Slope Roughness Type OR1\_1 SU1 J1 CONDUIT 10.0 3.0014 0.0130 OR1\_2 J1 OF1 ORIFICE \*\*\*\*\*\* Cross Section Summary \*\*\*\*\*\*\*

Full

Full

Hyd.

Max. No. of

Full

Conduit	Shape	Depth	Area	Rad.	Width	Barrels	Flow
OR1 1	CIRCULAR	0.30	0.07	0.07	0.30	1	0 17

## \* \* \* \* \* \* \* \* \* \* \* \* \* \* \* \*

### Analysis Options \*\*\*\*\*

Flow Units ..... CMS

Process Models:

Rainfall/Runoff ..... YES RDII ..... NO Snowmelt ..... NO Groundwater ..... NO Flow Routing ..... YES Ponding Allowed ..... YES Water Quality ..... NO Infiltration Method ..... HORTON Flow Routing Method ..... DYNWAVE Surcharge Method ..... EXTRAN Starting Date ..... 04/29/2024 00:00:00 Ending Date ...... 04/30/2024 00:00:00 Antecedent Dry Days ..... 0.0 Report Time Step ...... 00:01:00

Wet Time Step ...... 00:05:00 Dry Time Step ...... 00:05:00 Routing Time Step ..... 0.50 sec Variable Time Step ..... YES Maximum Trials ..... 8 Number of Threads ..... 1

Head Tolerance ..... 0.001500 m

* * * * * * * * * * * * * * * * * * * *	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
*******		
Total Precipitation	0.054	81.587
Evaporation Loss	0.000	0.000
Infiltration Loss	0.001	1.801
Surface Runoff	0.051	78.015
Final Storage	0.001	2.252
Continuity Error (%)	-0.589	
******	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr
******		
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.051	0.515
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	0.033	0.331
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000

Final Stored Volume ..... 0.018 0.183
Continuity Error (%) ..... 0.181

None

All links are stable.

Convergence obtained at all time steps.

Minimum Time Step 0.50 sec 0.50 sec Average Time Step Maximum Time Step 0.50 sec % of Time in Steady State : Average Iterations per Step: 2.02 % of Steps Not Converging : 0.01 Time Step Frequencies 0.500 - 0.500 sec : 100.00 % 0.500 - 0.500 sec 0.00 %

Total Total Total Peak Runoff Total Total Imperv Perv Total Precip Runon Evap Infil Runoff Runoff Runoff Runoff Coeff Runoff Subcatchment 10^6 ltr mm mm mm mm mm mm mm \_\_\_\_\_\_ 81.59 0.00 1.80 78.01 0.26 0.956

.\_\_\_\_\_

		Depth	Depth	HGL	Occurrence	Max Depth
Node	Type	Meters	Meters	Meters	days hr:min	Meters
J1	JUNCTION	2.45	3.42	179.02	0 02:49	3.42
OF1	OUTFALL	2.80	2.87	177.97	0 01:45	2.87
SU1	STORAGE	2.16	3.12	179.02	0 02:49	3.12

\_\_\_\_\_\_ Maximum Maximum Lateral Total Lateral Total Time of Max Inflow Inflow Balance Inflow Inflow Occurrence Volume Volume Error Node Type CMS CMS days hr:min 10^6 ltr 10^6 ltr Percent \_\_\_\_\_\_ JUNCTION 0.000 0.014 0 02:55 0 0.331 0.073 J1 0.000 0.014 0 02:55 0 0.331 0.000 OF1 OUTFALL 0.262 0.262 0 01:45 SU1 STORAGE 0.515 0.515 0.272

Surcharging occurs when water rises above the top of the highest conduit.

May Height Min Denth

			Max. Height	Min. Depth
		Hours	Above Crown	Below Rim
Node	Type	Surcharged	Meters	Meters
J1	JUNCTION	23.20	3.118	0.082

No nodes were flooded.

Average Avg Evap Exfil Maximum Max Time of Max Maximum Volume Pcnt Pcnt Pcnt Volume Pcnt Occurrence Outflow Storage Unit 1000 m³ Full Loss Loss 1000 m³ Full days hr:min CMS

 \*\*\*\*\*\*

	Flow	Avg	Max	Total
	Freq	Flow	Flow	Volume
Outfall Node	Pcnt	CMS	CMS	10^6 ltr
OF1	30.67	0.012	0.014	0.331
System	30.67	0.012	0.014	0.331

Link	Type	Maximum  Flow  CMS	Time of Max Occurrence days hr:min	Maximum  Veloc  m/sec	Max/ Full Flow	Max/ Full Depth
OR1_1 OR1_2	CONDUIT ORIFICE	0.014	0 02:55 0 02:55	0.29	0.09	1.00

	Adjusted			Fract	ion of	Time	in Flo	w Clas	s	
Conduit	/Actual Length	Dry	Up Dry		Sub Crit	-	-			Inlet Ctrl
OR1 1	1.00	0.02	0.00	0.00	0.97	0.00	0.00	0.00	0.01	0.00

Conduit		Hours Full Upstream		Hours Above Full Normal Flow		
OR1_1	22.71	22.71	23.20	0.01	0.01	

Analysis begun on: Wed May 8 12:28:08 2024 Analysis ended on: Wed May 8 12:28:08 2024

Total elapsed time: < 1 sec

# WQT Output Files

	R MANAGEMENT MODEL		uild 5.2.4	)			
*****							
Element Count *******							
Number of rain	gages 1						
Number of subca							
Number of nodes Number of links							
Number of pollu							
Number of land							
*****	•*						
Raingage Summar							
			Data	Recordin			
Name	Data Source		Туре	Interval			
Raingage	WQT		INTENSI				
*****	****						
Subcatchment Su	_						
Name	Area	Width %Imper	cv %Slop	pe Rain Gage		Outlet	
S1	0.66	85.71 90.0	00 1.00	00 Raingage		SU1	
****							
Node Summary							
* * * * * * * * * * *							
Name	Туре	Invert Elev.	Max. Depth	Area	External Inflow		
J1	JUNCTION	175.60	3.50	0.0			
OF1	OUTFALL	175.10	0.00	0.0			
SU1	STORAGE	175.90	3.20	0.0			
*****							
Link Summary							
**********	From Node	To Node	Time	T 022	+h %01.	ne Poughnoss	
Name	rrom Node	To Node	Туре	Leng		ope Roughness	
OR1_1	SU1	J1	CONDUIT	10	.0 3.00	0.0130	
OR1_2	J1	OF1	ORIFICE				
*****	****						
Cross Section S							
******	*****						

Full Full Hyd. Max. No. of Full

Conduit	Shape	Depth	Area	Rad.	Width	Barrels	Flow
OR1 1	CIRCULAR	0.30	0.07	0.07	0.30	1	0.17

## \* \* \* \* \* \* \* \* \* \* \* \* \* \* \* \*

#### Analysis Options \*\*\*\*\*

Flow Units ..... CMS

Process Models:

Rainfall/Runoff ..... YES RDII ..... NO Snowmelt ..... NO Groundwater ..... NO Flow Routing ..... YES Ponding Allowed ..... YES Water Quality ..... NO Infiltration Method ..... HORTON Flow Routing Method ..... DYNWAVE Surcharge Method ..... EXTRAN Starting Date ..... 04/29/2024 00:00:00 Ending Date ...... 04/30/2024 00:00:00 Antecedent Dry Days ..... 0.0

Report Time Step ...... 00:01:00 Wet Time Step ...... 00:05:00 Dry Time Step ...... 00:05:00 Routing Time Step ..... 0.50 sec Variable Time Step ..... YES Maximum Trials ..... 8

Number of Threads ..... 1

Head Tolerance ..... 0.001500 m

******	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
******		
Total Precipitation	0.021	31.995
Evaporation Loss	0.000	0.000
Infiltration Loss	0.001	1.694
Surface Runoff	0.019	28.256
Final Storage	0.001	2.252
Continuity Error (%)	-0.648	
*****	Volume	Volume
		10^6 ltr
Flow Routing Continuity	hectare-m	10.0 111
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.000	0.186
Groundwater Inflow	0.019	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	0.000	0.186
	0.019	0.000
Flooding Loss	0.000	0.000
Evaporation Loss  Exfiltration Loss	0.000	0.000
	0.000	
Initial Stored Volume	0.000	0.000

Final Stored Volume ..... 0.000 0.000 Continuity Error (%) ..... 0.000

All links are stable.

Convergence obtained at all time steps.

Minimum Time Step 0.50 sec 0.50 sec Average Time Step Maximum Time Step 0.50 sec % of Time in Steady State : Average Iterations per Step: 2.00 % of Steps Not Converging : 0.00 Time Step Frequencies 0.500 - 0.500 sec : 100.00 % 0.500 - 0.500 sec 0.00 %

Total Total Peak Runoff Total Total Imperv Perv Total Total Precip Runon Evap Infil Runoff Runoff Runoff Runoff Coeff Runoff Subcatchment 10^6 ltr CMS mm mm mm mm mm mm mm \_\_\_\_\_\_ 31.99 0.00 1.69 26.72 28.26 0.19 0.10 0.883

.\_\_\_\_\_

		Depth	Depth	HGL	Occurrence	Max Depth
Node	Type	Meters	Meters	Meters	days hr:min	Meters
J1	JUNCTION	0.14	1.16	176.76	0 02:09	1.16
OF1	OUTFALL	0.00	0.00	175.10	0 00:00	0.00
SU1	STORAGE	0.09	0.86	176.76	0 02:09	0.86

\_\_\_\_\_\_ Lateral Total Maximum Maximum Lateral Total Time of Max Inflow Inflow Balance Inflow Inflow Occurrence Volume Volume Error Node Type CMS CMS days hr:min 10^6 ltr 10^6 ltr Percent \_\_\_\_\_\_ JUNCTION 0.000 0.015 0 02:09 0 0.186 -0.001 J1 0.000 0.015 0 02:09 0 0.186 0.000 OF1 OUTFALL

0.186

0.186

-0.001

0.102 0.102 0 01:45

SU1

Surcharging occurs when water rises above the top of the highest conduit.

Max. Height Min. Depth

STORAGE

Node	Туре	Hours Surcharged	Above Crown Meters	Below Rim Meters
J1	JUNCTION	4.26	0.860	2.340

No nodes were flooded.

Average Avg Evap Exfil Maximum Max Time of Max Maximum Volume Pcnt Pcnt Pcnt Volume Pcnt Occurrence Outflow Storage Unit 1000 m³ Full Loss Loss 1000 m³ Full days hr:min CMS

 \*\*\*\*\*

	Flow	Avg	Max	Total
	Freq	Flow	Flow	Volume
Outfall Node	Pcnt	CMS	CMS	10 <b>^</b> 6 ltr
OF1	35.60	0.006	0.015	0.186
System	35.60	0.006	0.015	0.186

Link	Туре	Maximum  Flow  CMS	Time of Max Occurrence days hr:min	Maximum  Veloc  m/sec	Max/ Full Flow	Max/ Full Depth
OR1_1 OR1_2	CONDUIT ORIFICE	0.015 0.015	0 02:09 0 02:09	0.41	0.09	1.00

	Adjusted			 Fract	ion of	Time	 in Flo	 w Clas	s	
Conduit	/Actual Length	Dry	Up Dry		Sub Crit	-	-			
OR1_1	1.00	0.04	0.00	0.00	0.68	0.28	0.00	0.00	0.78	0.00

				Hours	Hours
		Hours Full		Above Full	Capacity
Conduit	Both Ends	Upstream	Dnstream	Normal Flow	Limited
OR1_1	2.96	2.96	4.26	0.01	0.01

Analysis begun on: Wed May 8 12:39:30 2024 Analysis ended on: Wed May 8 12:39:30 2024

Total elapsed time: < 1 sec

# Climate Change Stress Test Output Files

DR1_1 DR1_2	SU1 J1	J1 OF1		CONDUIT	1	0.0	3.0014	0.0130	
Name 	From Node	To Node	T 		Leng	gth <sup>9</sup>	Slope	Roughness	
Link Summary									
****									
SU1	STORAGE	175.	90	3.20	0.0				
DF1	OUTFALL	175.	10	0.00	0.0				
 Г1	JUNCTION	175.		3.50	0.0				
Name	Туре	Inve: Ele	v.	Max. Depth	Ponded Area	Externa Inflow	3.1		
*****		<b>T</b>	-a+	Mo	Donder	<b>R</b>	. 1		
************ Node Summary									
51	0.66	85.71	90.00	1.0000	Raingage		Ş	SU1	
Jame 	Area	Width %	Imperv	%Slop∈	Rain Gage	e 		Outlet 	
Subcatchment Sun									
*****	* * * * *								
Raingage	ClimateChange	2		INTENSITY	15 min				
Name 	Data Source			Data Type	Recording Interval				
Raingage Summary									
*****	•								
Number of nodes Number of links Number of pollut Number of land u	2 cants 0								
Number of rain o									
Element Count									

Full Full Hyd. Max. No. of Full

Conduit	Shape	Depth	Area	Rad.	Width	Barrels	Flow
OR1 1	CIRCULAR	0.30	0.07	0.07	0.30	1	0.17

## \* \* \* \* \* \* \* \* \* \* \* \* \* \* \* \*

#### Analysis Options \*\*\*\*\*

Flow Units ..... CMS

Process Models:

Rainfall/Runoff ..... YES RDII ..... NO Snowmelt ..... NO Groundwater ..... NO Flow Routing ..... YES Ponding Allowed ..... YES Water Quality ..... NO Infiltration Method ..... HORTON Flow Routing Method ..... DYNWAVE Surcharge Method ..... EXTRAN Starting Date ..... 04/29/2024 00:00:00 Ending Date ...... 04/30/2024 00:00:00 Antecedent Dry Days ..... 0.0 Report Time Step ...... 00:01:00

Wet Time Step ...... 00:05:00 Dry Time Step ...... 00:05:00 Routing Time Step ..... 0.10 sec Variable Time Step ..... YES Maximum Trials ..... 8 Number of Threads ..... 1

Head Tolerance ..... 0.001500 m

*******	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
* * * * * * * * * * * * * * * * * * * *		
Total Precipitation	0.075	114.223
Evaporation Loss	0.000	0.000
Infiltration Loss	0.001	1.829
Surface Runoff	0.073	110.783
Final Storage	0.001	2.252
Continuity Error (%)	-0.562	
*******	Volume	Volume
Flow Routing Continuity	hectare-m	10 <b>^</b> 6 ltr
*******		
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.073	0.731
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	0.055	0.547
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.000	0.000

Final Stored Volume ..... 0.018 0.183 Continuity Error (%) ..... 0.079

Link OR1\_2 (4)

Convergence obtained at all time steps.

Minimum Time Step 0.10 sec 0.10 sec Average Time Step Maximum Time Step 0.10 sec % of Time in Steady State : Average Iterations per Step: 2.19 % of Steps Not Converging : 1.05 Time Step Frequencies 0.100 - 0.100 sec : 100.00 % 0.100 - 0.100 sec 0.00 % 0.100 - 0.100 sec 0.00 % 0.100 - 0.100 sec 0.00 %

0.100 - 0.100 sec

Total Total Peak Runoff Total Total Imperv Perv Total Total Runoff Precip Runon Evap Infil Runoff Runoff Runoff Coeff Runoff Subcatchment 10^6 ltr CMS mm mm mm mm mm mm mm \_\_\_\_\_\_ 114.22 0.00 1.83 101.12 9.67 110.78 0.73 0.37 0.970

-----

0.00 %

		Depth	Depth	HGL	0ccu	rrence	Max Depth
Node	Type	Meters	Meters	Meters	days	hr:min	Meters
J1	JUNCTION	2.69	6.50	182.10	0	02:28	6.48
OF1	OUTFALL	2.80	2.90	178.00	0	01:40	2.90
SU1	STORAGE	2.40	6.20	182.10	0	02:28	6.20

Maximum Maximum Lateral Total Flow
Lateral Total Time of Max Inflow Inflow Balance
Inflow Inflow Occurrence Volume Volume Error

		Lateral	Total	Time of Max	Inflow	Inflow	Balance
		Inflow	Inflow	Occurrence	Volume	Volume	Error
Node	Type	CMS	CMS	days hr:min	10^6 ltr	10 <b>^</b> 6 ltr	Percent
J1	JUNCTION	0.000	0.028	0 02:32	0	0.547	-0.023
OF1	OUTFALL	0.000	0.028	0 02:32	0	0.547	0.000
SU1	STORAGE	0.368	0.368	0 01:45	0.731	0.731	0.194

Surcharging occurs when water rises above the top of the highest conduit.

Max. Height Min. Depth

Node	Туре	Hours Surcharged	Above Crown Meters	Below Rim  Meters
J1	JUNCTION	23.36	6.200	0.000
SU1	STORAGE	22.87	5.900	

Flooding refers to all water that overflows a node, whether it ponds or not.

\_\_\_\_\_ Total Maximum Maximum Time of Max Flood Ponded Hours Rate Occurrence Volume Depth CMS days hr:min 10^6 ltr Node Flooded Meters \_\_\_\_\_ J1 0.01 0.000 0 02:28 0.000 3.000 SU1 0.06 0.012 0 02:28 0.000 3.000

------

	Average	Avg	Evap	Exfil	Maximum	Max	Time of Max	Maximum
	Volume	Pcnt	Pcnt	Pcnt	Volume	Pcnt	Occurrence	Outflow
Storage Unit	1000 m <sup>3</sup>	Full	Loss	Loss	1000 m³	Full	days hr:min	CMS
SU1	0.274	46.8	0.0	0.0	0.586	100.0	0 02:28	0.028

Flow Avg Max Total
Freq Flow Flow Volume
Outfall Node Pcnt CMS CMS 10^6 ltr

OF1 45.46 0.014 0.028 0.547

System

 Maximum
 Time of Max
 Maximum
 Max/mum
 Max/ Max/

 |Flow|
 Occurrence
 |Veloc|
 Full
 Full

 Link
 Type
 CMS
 days hr:min
 m/sec
 Flow
 Depth

 OR1\_1
 CONDUIT
 0.028
 0 02:32
 0.40
 0.17
 1.00

 OR1\_2
 ORIFICE
 0.028
 0 02:32
 1.00

45.46 0.014 0.028 0.547

| Hours | Hour

Analysis begun on: Thu May 9 10:35:04 2024 Analysis ended on: Thu May 9 10:35:05 2024

Total elapsed time: 00:00:01







## **ADS OGS Sizing Summary**

Project Name: 0 Esplanade Dr.

Consulting Engineer: Dillon Consulting

**Location:** Windsor, ON

Sizing Completed By: C. Neath Email: <a href="mailto:cody.neath@adspipe.com">cody.neath@adspipe.com</a>

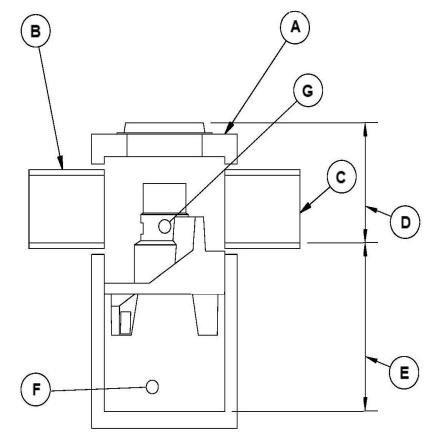
Treatment Requirements					
Treatment Goal: Normal (MOE)					
Selected Parameters:	70% TSS 90% Volume				
Selected Unit:	FD-4HC				

Summary of Results						
Model	TSS Removal	<b>Volume Treated</b>				
FD-4HC	76.0%	>90%				
FD-5HC	84.0%	>90%				
FD-6HC	86.0%	>90%				
FD-8HC	91.0%	>90%				
FD-10HC	94.0%	>90%				

FD-4HC Specification						
Unit Diameter (A):	1,200 mm					
Inlet Pipe Diameter (B):	300 mm					
Outlet Pipe Diameter (C):	300 mm					
Height, T/G to Outlet Invert (D):	2000 mm					
Height, Outlet Invert to Sump (E):	1515 mm					
Sediment Storage Capacity (F):	0.78 m³					
Oil Storage Capacity (G):	723 L					
Recommended Sediment Depth for Maintenance:	440 mm					
Max. Pipe Diameter:	600 mm					
Peak Flow Capacity:	510 L/s					

Site Elevations:						
Rim Elevation:	100.00					
Inlet Pipe Elevation:	98.00					
Outlet Pipe Elevation:	98.00					

Site Details						
Site Area:	0.66 ha					
% Impervious:	90%					
Rational C:	0.84					
Rainfall Station:	Windsor, ONT					
Particle Size Distribution:	Fine					
Peak Flowrate:						



#### Notes:

Removal efficiencies are based on NJDEP Test Protocols and independently verified.

All units supplied by ADS have numerous local, provincial, and international certifications (copies of which can be provided upon request). The design engineer is responsible for ensuring compliance with applicable regulations.



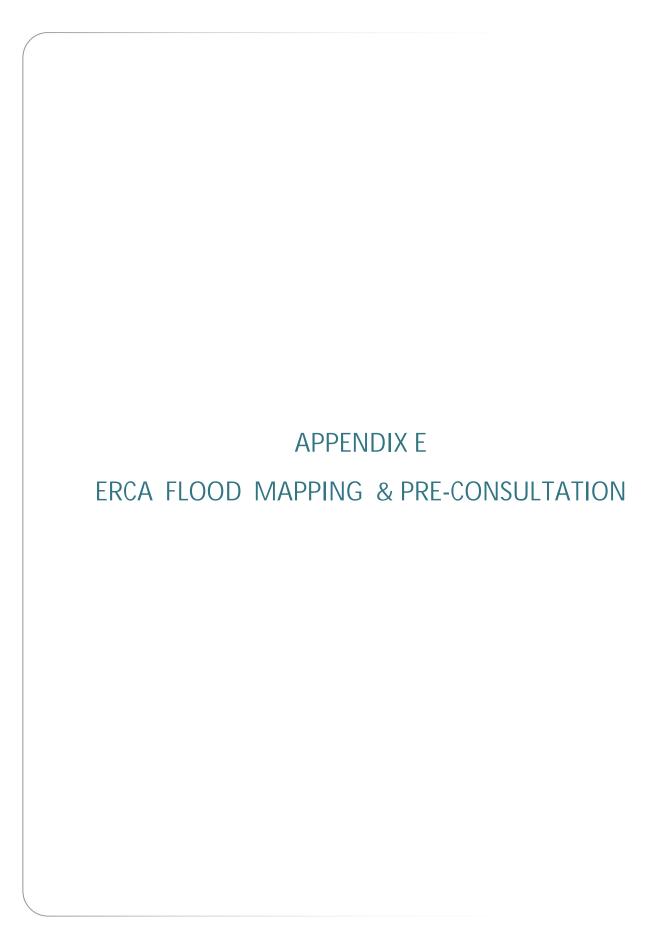
Project Name: 0 Esplanade Dr.
Consulting Engineer: Dillon Consulting
Location: Windsor, ON

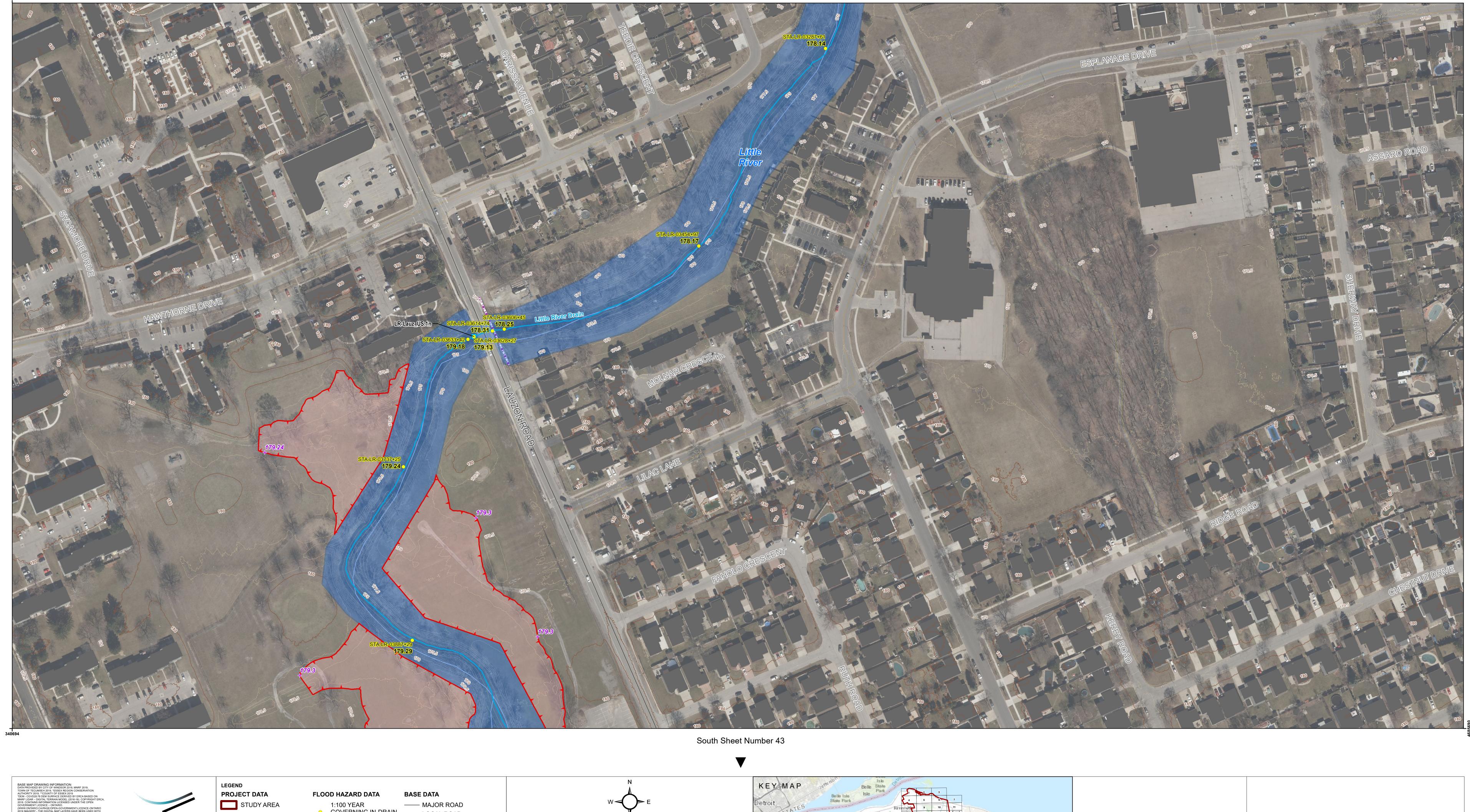
## Net Annual Removal Efficiency Summary: FD-4HC

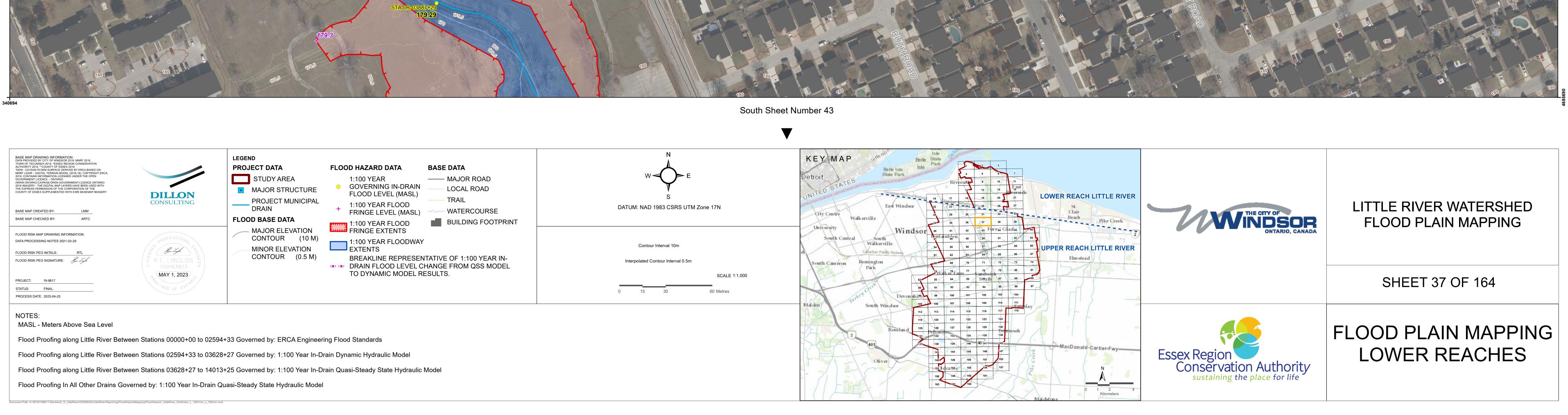
Rainfall Intensity <sup>(1)</sup>	Rational Equation Flowrate	Surface Loading Rate	Fraction of Rainfall <sup>(1)</sup>	FD-4HC Removal Efficiency	Weighted Net- Annual Removal Efficiency
mm/hr	L/s	L/min/m <sup>2</sup>	%	%	%
3.00	4.6	245	13.2%	90%	11.9%
4.00	6.2	327	9.6%	88%	8.4%
5.00	7.7	408	7.5%	86%	6.5%
6.00	9.2	490	6.0%	85%	5.1%
7.00	10.8	572	4.8%	83%	4.0%
8.00	12.3	654	4.1%	82%	3.4%
9.00	13.9	735	3.6%	81%	2.9%
10.00	15.4	817	3.2%	81%	2.6%
11.00	16.9	899	2.8%	80%	2.2%
12.00	18.5	980	2.5%	79%	2.0%
15.00	23.1	1225	6.6%	78%	5.1%
20.00	30.8	1634	8.3%	76%	6.3%
25.00	38.5	2042	5.8%	74%	4.3%
30.00	46.2	2451	4.6%	73%	3.3%
35.00	53.9	2859	3.8%	72%	2.7%
40.00	61.6	3268	2.9%	71%	2.1%
45.00	69.3	3676	2.4%	70%	1.7%
50.00	77.0	4085	1.8%	69%	1.2%
65.00	100.1	5310	6.6%	0%	0.0%
	Total Net Annual Removal Efficiency:				
	Total Runoff Volume Treated:				

### Notes:

- (1) Based on Windsor/Essex Region Stormwater Manual 2018, Table 3.4.1.5
- (2) Based on third party verified data and appoximating the removal of a PSD similar to the STC Fine distribution









Jeyalakshmi, Saranya <sjeyalakshmi@dillon.ca>

## Fwd: FW: SWM/Floodproofing requirements for 0 Esplanade Drive, Windsor

1 message

Bagchi, Aakash <abagchi@dillon.ca>

To: Saranya Jeyalakshmi <sjeyalakshmi@dillon.ca>

Tue, Sep 3, 2024 at 10:11 AM

Please see the floodproofing elevation from ERCA for 0 Esplanade below. It needs to be updated in the SWM Report.





Aakash Bagchi

Associate
Dillon Consulting Limited
3200 Deziel Drive Suite 608
Windsor, Ontario, N8W 5K8
T - 519.948.5000 ext. 3235
ABagchi@dillon.ca
www.dillon.ca

WE'RE MOVING! - On October 1, 2024 our office will be relocating to 1 Riverside Drive West, Windsor ON, N9A 5K3 Upcoming Vacation: September 5-6; September 30-October 4 (dates inclusive)

------From: **Tian Martin** <TMartin@erca.org>
Date: Wed, Aug 28, 2024 at 1:34 PM

Subject: FW: SWM/Floodproofing requirements for 0 Esplanade Drive, Windsor

To: Bagchi, Aakash <abagchi@dillon.ca> Cc: Amy Farkas <afarkas@dillon.ca>

Apologies, please see the correction below.

From: Tian Martin

**Sent:** Wednesday, August 28, 2024 12:19 PM **To:** Bagchi, Aakash <abaqchi@dillon.ca> **Cc:** Amy Farkas <afarkas@dillon.ca>

Subject: RE: SWM/Floodproofing requirements for 0 Esplanade Drive, Windsor

Hi Aakash,

Based on the Little River Flood Hazard Map 37 attached, the nearest 1:100 year water level in the Little River is 178.14m CGVD28:78, therefore the minimum building opening elevation will be 178.48 178.44m CGVD28:78, or 0.30m above the 1:100 year WSEL on-site, or the Stress Test WSEL on-site.

Based on the information provided, the anticipated outlet being the city storm sewer and the design being in accordance with the regional SWM guidelines, ERCA does not foresee any further stormwater related

requirements at this time.

#### Thanks,



#### TIAN MARTIN, P.Eng.

Water Resources Engineer, Watershed Management Services

**Essex Region Conservation Authority** 

360 Fairview Avenue West, Suite 311 Ÿ Essex, Ontario Ÿ N8M 1Y6

P. 519-776-5209 x 304 Ÿ F. 519-776-8688

tmartin@erca.org www.essexregionconservation.ca

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Follow us on Twitter: @essexregionca

From: Bagchi, Aakash <abagchi@dillon.ca>
Sent: Tuesday, August 27, 2024 4:11 PM
To: Tian Martin <TMartin@erca.org>
Cc: Amy Farkas <afarkas@dillon.ca>

Subject: SWM/Floodproofing requirements for 0 Esplanade Drive, Windsor

Good Afternoon Tian,

Dillon is assisting with a proposed development in Windsor, located at 0 Esplanade Drive. A map showing the location is attached for reference. The City of Windsor has requested consultation with ERCA regarding floodproofing and other design requirements that may affect the SWM design.

Can you please confirm the floodproofing requirements for this development?

Based on our knowledge of the watershed, the following will apply:

- The 100-year water level in Little River at the nearest point to the site (upstream of Tecumseh road crossing) in the Little River Watershed Flood Line Mapping Final Hydraulic Report (Dillon, 2023) is 178.08 m.
- Therefore, the minimum building opening will be 178.38 m, or 0.30 m above 100-Year WSEL on-site, or Climate Change stress test WSEL on-site, whichever is greater.

Can you also confirm if there are any other design requirements related to stormwater management that we should take into account for this site?

The proposed stormwater outlet for this site will be a storm trunk sewer that passes through the site in a municipal easement, eventually draining to Little River. The preliminary SWM design requires underground as well as surface storage to meet the requirements of the regional SWM guidelines.

Thank you,

Aakash





Aakash Bagchi
Associate
Dillon Consulting Limited
3200 Deziel Drive Suite 608
Windsor, Ontario, N8W 5K8
T - 519.948.5000 ext. 3235
ABagchi@dillon.ca

WE'RE MOVING! - On October 1, 2024 our office will be relocating to 1 Riverside Drive West, Windsor ON, N9A 5K3

Upcoming Vacation: September 5-6; September 30-October 4 (dates inclusive)

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#### 2 attachments



FloodHazard\_LittleRiver\_GridIndex\_L\_1067mm\_x\_762mm\_37.pdf 8964K