



Ganatchio Gardens Inc.

Official Plan and Zoning By-Law Amendments

Stormwater Management Report

Southwest Corner of Florence Avenue & Wyandotte Street East
Windsor, Ontario

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1.0

Introduction

Dillon Consulting Limited (Dillon) has been retained by Ganatchio Gardens Inc. to complete the detailed design for a proposed multi-storey residential development in the City of Windsor. This Stormwater Management Report has been prepared to support the detailed design of the proposed development.

The proposed development consists of 275 multi-unit residential buildings and 28 townhome residential buildings. The total site area is 3.30 ha (8.15 ac) and is located in the City of Windsor at the south west corner of Wyandotte Street and the proposed Florence Avenue extension. The proposed development will drain into the existing 1.95 m diameter storm sewer main along the west boundary of the site that conveys flows south and drains into a storm water management pond south west of the development site. Under existing conditions, the site is undeveloped and consists of grassed land cover. The general slope of the ground directs flows northwards. The location and the layout of the site boundary is shown in Figure 1 and the site plan is in Appendix A



Figure 1: Project Site Location

The purpose of this report is to assess the storm water management requirements for the proposed development while restricting the peak outflow from the site to an allowable release rate. Storage on-site is to be recommended to attenuate peak flow rates for all events, including the governing 1:100 year event and the Urban Stress Test.

1.1 Background

In 2018, Dillon completed a storm water assessment study of the North Neighbourhood Development for the City of Windsor (the City). The details of the previously completed study can be found in the North Neighbourhood Development Storm Water Management Analysis Report (Dillon 2018). The current development was part of the ultimate future build out area considered in the 2018 study. As such, the currently proposed development was assessed to the North Neighbourhood SWM Pond and the Wyandotte Street storm sewer.

1.2 SWM Design Criteria

Design criteria for the stormwater design and servicing were based on review of the following reference documents:

- Stormwater Management Planning and Design Manual (Ministry of the Environment [MECP], 2003);
- Windsor/Essex Region Stormwater Management Standards Manual (WERSMSM) (2018); and
- North Neighbourhood Stormwater Management Study (Dillon, 2018).

The corresponding criteria are described below.

1.2.1 Quantity Control

1.2.1.1 Minor System Conveyance

Hydraulic Grade Lines in the minor system have been assessed for the 1:5 year 4 hour storm (with 15 minute time intervals and using the Chicago distribution). Storm sewers have been designed to allow minimal surcharging, where the HGL is below the lowest catch-basin (CB) grate elevation.

1.2.1.2 Climate Change Resiliency Assessment

The stormwater management system's performance has been examined under conditions more intense than the 1:100 year design storm event to assess potential impacts of climate change and the system's resiliency using the Urban Stress Test design storm event. As far as possible, provided surrounding grades allow, the site grading is designed to contain the runoff generated from this design storm event without overflowing onto neighbouring properties or right-of-way (ROW).

The following design storm events were used for the analysis:

- 1:5 year 4 hour design storm using Chicago distribution with a 15 minute time interval and a total rainfall depth of 49.5 mm.
- 1:100 year 4 hour design storm using Chicago distribution with 15 minute time interval with a total rainfall depth of 81.6 mm. Used to assess the major system HGL corresponds to a maximum surface ponding of 0.3 m depth.
- 1:100 year 24 hour design storm using SCS Type-II distribution with a 2 hour time interval and a total rainfall depth of 108 mm. Used to assess the major system HGL corresponds to a maximum surface ponding of 0.3 m depth.
- 1:100 year 24 hour design storm using Chicago distribution with 15 minute time interval and an additional 42 mm uniformly distributed, with a total rainfall depth of 150 mm - Urban Stress Test Storm.

1.2.2 Quality Control

Since the subject development lands result in an increase in paved surface in the development area, measures have to be undertaken to treat the quality of the stormwater runoff being discharged into receiving watercourses/sewers. Stormwater quality treatment will be provided using an oil-grit separator (OGS) positioned upstream of the outlet storm sewer. The OGS unit is designed to meet the Ministry of Environment, Conservation and Parks (MECP) design requirements for 70% TSS removal (normal level of protection).

2.0

Allowable Release Rate

The subject development lands were assessed to the Wyandotte Street storm sewer in the 2018 North Neighbourhood Study. In the proposed conditions PCSWMM model set up as part of this study, the development lands were included with an imperviousness percentage of 55%.

As such, the release rate of the proposed site was estimated considering a percentage imperviousness of 55% in the modelling analysis. The estimated maximum allowable stormwater flow release rates for the subject site is 457 L/s. This is the 1:5 year, 4 hour design storm event, post-development peak flow rate from the subject site.

In order to prevent any adverse impacts on the downstream system due to the proposed development, the maximum flow rate from the site is expected to be maintained at or below the allowable release rate for all events up to and including the 1:100 year event.

2.1

Downstream Capacity Analysis

The PCSWMM model developed as part of the North Neighbourhood Stormwater Management Study (Dillon, 2018) was utilized to determine upstream and downstream impacts on the Wyandotte Street storm sewer system. The model was simulated using the 1:100 year 4 hour, 1:100 year 24 hour and the 1:5 year, 4 hour design storm events, with and without the inflow from the proposed development. Comparing the Hydraulic Grade Lines (HGLs) along Wyandotte, there was no observed increase in HGLs during the 1:5 year or the 1:100 year event simulations.

This is understood to be because the flows from the proposed development are a much smaller value compared to the peak flows in the larger Wyandotte Street storm sewer. Additionally, the proposed development is near the downstream end of the Wyandotte Street storm sewer system. The peak flow from the development occurs before the peak flows and HGLs in the Wyandotte St storm sewer occur due to a larger upstream drainage area of the 1.95 m diameter storm sewer on Wyandotte Street.

Therefore, it was concluded that the release rate from the proposed site will not have a significant impact on the receiving sewer system. Profiles of the Wyandotte Street sewer showing HGLs in the sewer, with and without the new development inflow, are included in Appendix C

3.0

Proposed Condition Analysis

3.1

Proposed Condition Hydrologic Assessment

Under proposed conditions, the 3.3 ha site area consists of 275 multi-unit residential buildings and 28 townhome residential buildings. Sub catchment attributes for the proposed development were selected based on the ERCA SWM standard and are summarized in below Table 1. Additional details of the modelling parameters and other model details for proposed conditions are provided in Appendix B

Table 1: Post Development Sub-Catchment Parameters for the Site

Attribute	Development
Land Use	Residential
Area (ha)	3.3
Flow Length* (m)	340
Imperviousness (%)	90
Slope (%)	1
Manning's n Impervious	0.013
Manning's n Pervious	0.24
Depression Storage Impervious (mm)	2.5
Depression Storage Pervious (mm)	7.5
Maximum Infiltration Rate (mm/hr)	75
Minimum Infiltration Rate (mm/hr)	0.5
Decay Constant (mm/hr)	4
Drying Time (days)	7

*Maximum flow path to outlet

3.1.1

Tail Water Conditions

The impact of downstream tailwater conditions occurring due to high Hydraulic Grade Line (HGL) elevations in the receiving Wyandotte Street storm sewer, on the site's stormwater management system was accounted for in the PCSWMM model. Head time-series were extracted from the North Neighbourhood Model for the 1:5 year, 4 hour; 1:100 year, 4 hour; 1:100 year, 24 hour and UST events, for the node MH 6R3879. These time-series were then applied to the outfall node in the proposed condition PCSWMM model to represent tail water conditions.

The head time series used to simulate tailwater conditions for different storm events are shown in Figure 2.

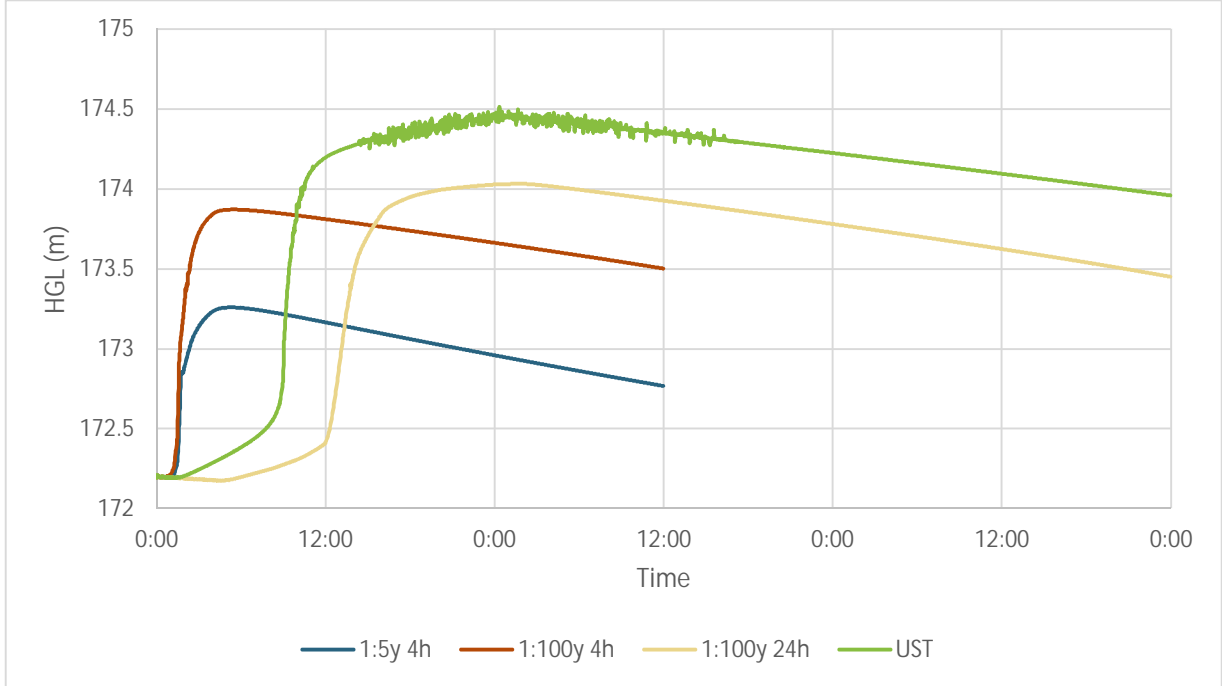


Figure 2: TW Time series for different storm events

3.2 Quantity Control

Stormwater storage on the site is proposed in the parking lot at catch-basin (CB) locations. A 675 mm diameter pipe and 480 mm circular orifice is proposed from the site to the outlet node (6R3879) to restrict the flow within the allowable rate.

The parking lot areas will be graded to include local sags at catch basin locations to allow for surface ponding during large storm events. Storage in the storm sewers and sewer structures has been taken into account in this analysis and incorporated into the stage-storage curve used to simulate on-site storage in the model.

The proposed condition model was simulated for different storm events. A summary of the surface storage depth and the on-site storage volume, along with the release rate for different storm event simulations is provided in below Table 2.



Table 2: Onsite Storage Depth, Storage Volume and Release for different Storms

Storm Type	Release Rate (m ³ /s)	Surface Storage Depth (m)	Storage Volume (m ³)
1:5 year 4 hour Chicago	0.41	0	540
1:100 year 4 hour Chicago	0.45	0.18	980
1:100 year 24 hour SCS Type-II	0.22	0	510
Urban Stress Test	0.45	0.20	1082

Based on the modelling analysis summarized in Table 2, it is observed that the available surface storage provides adequate storage for the site to restrict the flow rate within the allowable release rate and restrict estimated surface ponding depth to less than 0.3 m during 1:100 year storm events.

From the above table, it is also observed that the 1:100 year, 4 hour storm (Chicago) event is the governing 1:100 year return period event regarding storage requirements. The maximum volume of storm water estimated to be stored on-site is 980 m³, during the 1:100 year simulation. This corresponds to a maximum surface ponding depth of 0.18 m at CB locations. The details of the model inputs and outputs are provided in Appendix B

The Urban Stress Test (UST) storm event was also simulated to account for impacts of climate change. The estimated depth of storage during the UST event simulation shown in Table 3 is higher than the maximum estimated depth during the governing 1:100 year simulation and is estimated to be 0.20 m from the lowest CB grate elevation.

The flow from the site is conveyed via a 675 mm diameter conduit to the outfall (6R3879) of the Wyandotte Street East storm sewer system. Additionally, a 480 mm circular orifice is required to restrict the flow within the allowable limit.

3.3 Quality Control

As discussed in Section 1.2.2, the site will be required to meet Normal Protection Level water quality treatment (70% TSS removal). It is proposed that an oil and grit separator (OGS) unit be used to meet this target. The FD-4HC model supplied by ADS, or approved equivalent is recommended for this site. The details of this OGS sizing is provided in Appendix D

Conclusions

The stormwater management design for the proposed development meets the established SWM criteria for the overall site, and no negative impacts due to the site development are anticipated in the existing system.

Based on the analysis performed, the conclusions are listed as follows:

- The allowable release rate for this proposed development is estimated to be 0.457 m³/s. This is based on a 1:5 year post-development release from the development area, assuming a post-development percentage imperviousness of 55% for the site.
- Available parking lot storage and pipe storage is adequate for the site to restrict the flow within the allowable release rate during the 1:100 year storm event simulation without surface ponding exceeding 0.30 m.
- A 675 mm diameter circular pipe and 480 mm diameter circular orifice is proposed at the outlet to provide flow restriction for maintaining outflow within the allowable release rate.
- On-site storage volume of 980 m³ is required for the 1:100 year event to restrict flows from the site to the allowable release rate. This corresponds to a maximum estimated surface ponding depth of 0.18 m during this simulation.
- From the outlet capacity assessment analysis, no significant change in HGLs in the Wyandotte Street storm sewers, downstream of the development, is observed. Therefore, no negative impact to the hydraulic conditions of the downstream municipal sewer is expected due to the proposed development.
- Water quality control will be achieved through the use of an FD-4HC OGS unit to achieve 70% TSS removal over an average annual basis.

This report is respectfully submitted for review and approval. Should you have any questions, we would be pleased to discuss the results of our evaluation in further detail.

Yours sincerely,

DILLON CONSULTING LIMITED



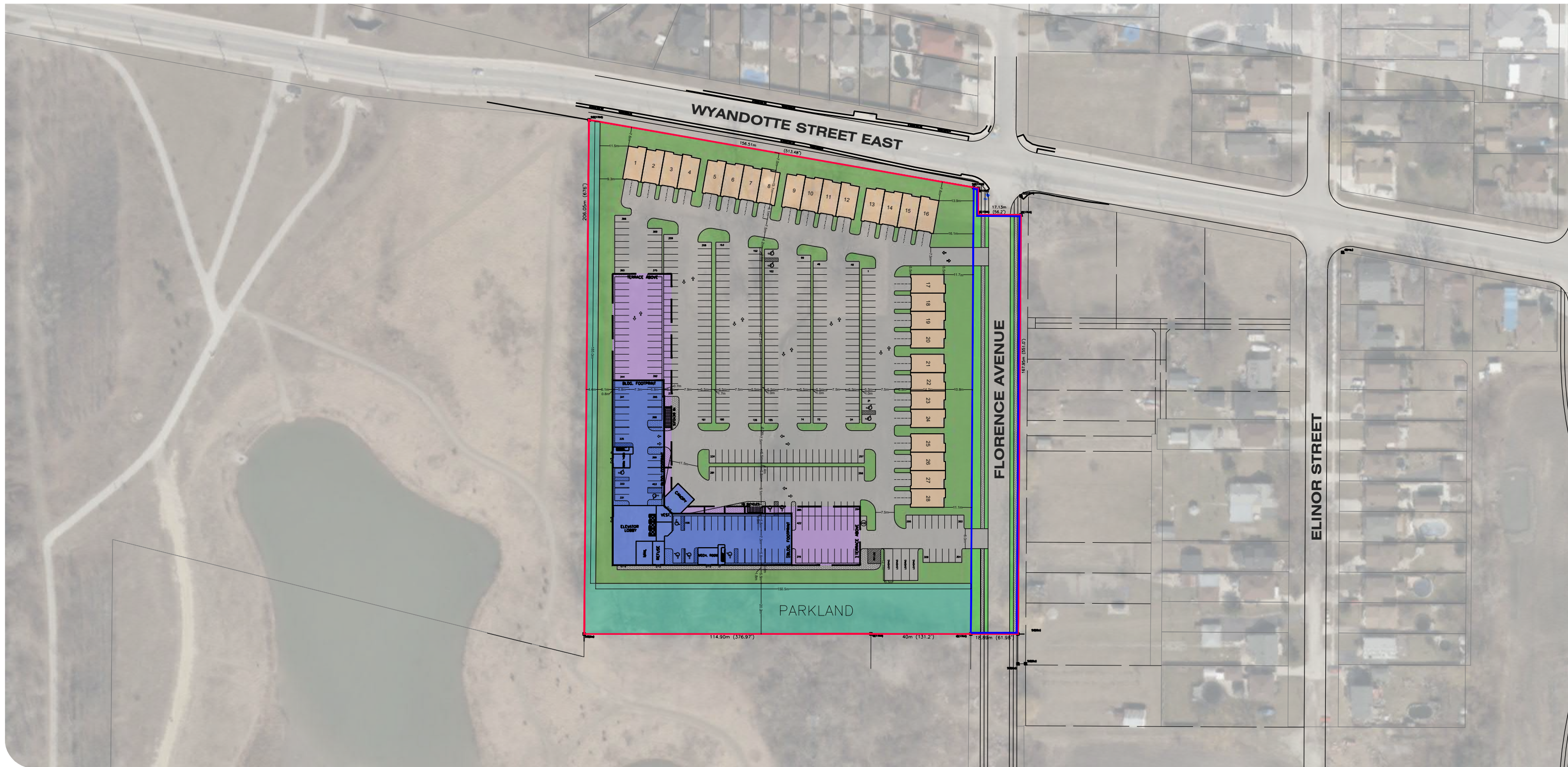
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Appendix A

Ganatchio Garden Site Plan



GANATCHIO GARDENS INC.
 WYANDOTTE STREET EAST
 AT FLORENCE AVENUE

CONCEPTUAL DEVELOPMENT PLAN
 FEBRUARY 16, 2023

- SUBJECT AREA
(± 3.30ha / 8.15ac)
- LAND CONVEYANCE
(± 0.32ha / 0.79ac)
- PROPOSED TOWNHOME UNITS (28 UNITS)
- PROPOSED PARKLAND
- PROPOSED MULTI-UNIT RESIDENTIAL BUILDING (275 UNITS)
- PROPOSED LANDSCAPING
- PROPOSED ELEVATED TERRACE
- PROPOSED SIDEWALK

UNIT COUNT

MULTI- UNIT RESIDENTIAL:	275 units
TOWNHOME:	28 units
TOTAL:	303 units

PARKING COUNT:

PARKING MULTI-UNIT:	: 432 SPACES
TOWNHOME (GARAGE, 2 / UNIT)	: 56 SPACES
TOWNHOME (SURFACE, 2 / UNIT)	: 56 SPACES
TOTAL	: 544 SPACES

PARKING DETAILS:

PARKING/UNIT RATIO (MULTI-UNIT)	: 1.57 SPACES / UNIT
PARKING/UNIT RATIO (TOWNHOME)	: 4 SPACES / UNIT
(GARAGE + SURFACE PARKING)	
LOADING SPACES	: 4 SPACES
ACCESSIBLE SPACES PROVIDED (TYPE A/TYP E B)	: 12 SPACES

File Location:
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 February, 16, 2023 3:08 PM

SOURCE: THE COUNTY OF ESSEX INTERACTIVE MAPPING (2019)

MAP/DRAWING INFORMATION
 THIS DRAWING IS FOR INFORMATION PURPOSES ONLY. ALL DIMENSIONS AND BOUNDARY INFORMATION SHOULD BE VERIFIED BY AN O.L.S PRIOR TO CONSTRUCTION.
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 CHECKED BY: MAM
 DESIGNED BY: MRU

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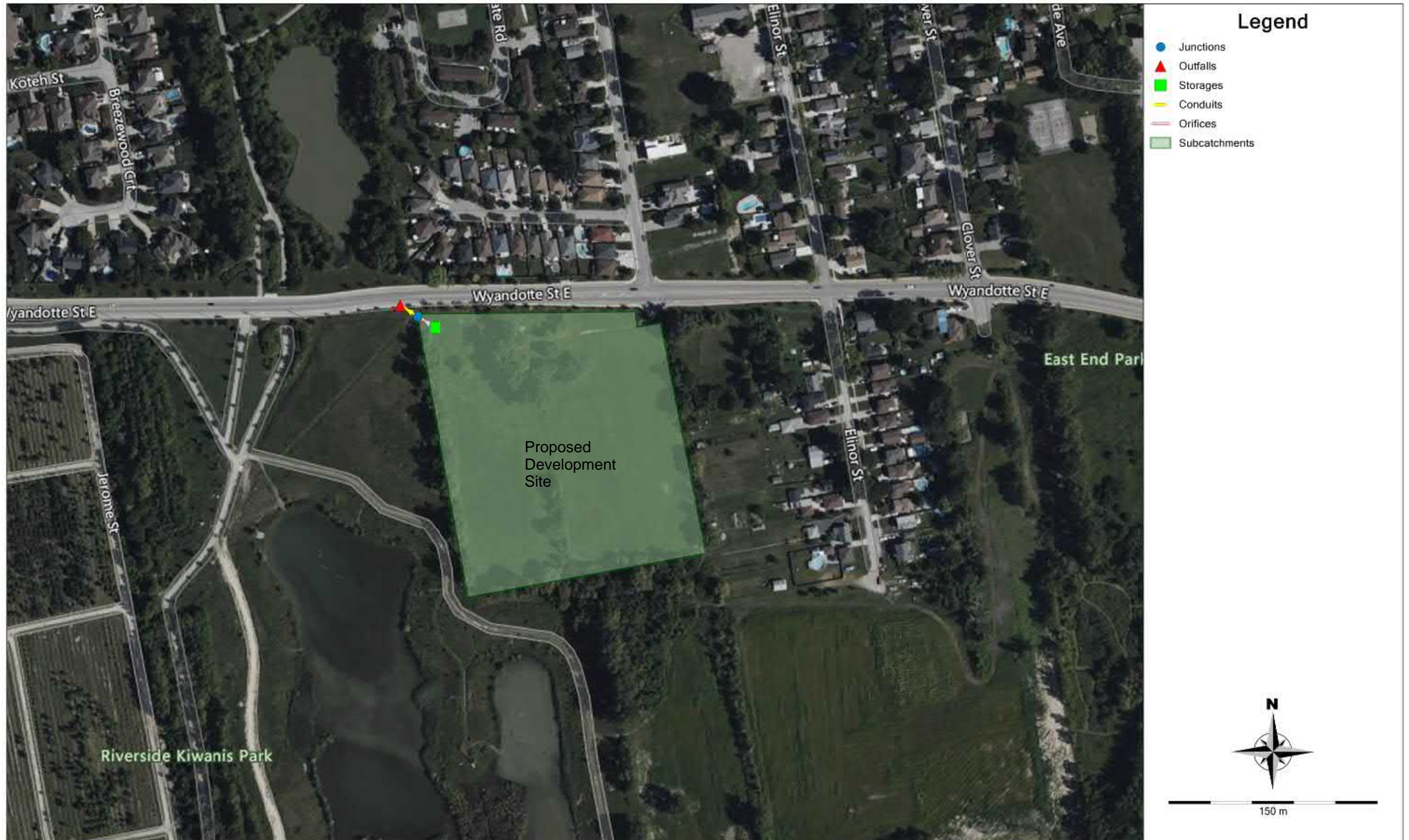


PROJECT: 21-1691
 STATUS: DRAFT
 DATE: 2023/02/10

Appendix B

Modelling Input and Output Reports

Model Schematic



PCSWMM Input Report

[TITLE]

;;Project Title/Notes

[OPTIONS]

;;Option Value
 FLOW_UNITS CMS
 INFILTRATION HORTON
 FLOW_ROUTING DYNWAVE
 LINK_OFFSETS DEPTH
 MIN_SLOPE 0
 ALLOW_PONDING NO
 SKIP_STEADY_STATE NO

START_DATE 04/11/2022
 START_TIME 00:00:00
 REPORT_START_DATE 04/11/2022
 REPORT_START_TIME 00:00:00
 END_DATE 04/12/2022
 END_TIME 12:00:00
 SWEEP_START 01/01
 SWEEP_END 12/31
 DRY_DAYS 0
 REPORT_STEP 00:01:00
 WET_STEP 00:05:00
 DRY_STEP 00:05:00
 ROUTING_STEP 1
 RULE_STEP 00:00:00

INERTIAL_DAMPING PARTIAL
 NORMAL_FLOW_LIMITED BOTH
 FORCE_MAIN_EQUATION H-W
 VARIABLE_STEP 0.75
 LENGTHENING_STEP 0
 MIN_SURFAREA 0
 MAX_TRIALS 8
 HEAD_TOLERANCE 0.0015
 SYS_FLOW_TOL 5
 LAT_FLOW_TOL 5
 MINIMUM_STEP 0.5
 THREADS 4

[EVAPORATION]

;;Data Source Parameters
 ;;-----
 CONSTANT 0.0
 DRY_ONLY NO

[RAINGAGES]

;;Name Format Interval SCF Source
 ;;-----
 Raingage1 INTENSITY 0:15 1.0 TIMESERIES 5y4h15mDistribution

[SUBCATCHMENTS]

;;Name	Rain Gage	Outlet	Area	%Imperv	Width	%Slope	CurbLen	SnowPack
;;-----	-----	-----	-----	-----	-----	-----	-----	-----
S1	Raingage1	SU1	3.2978	90	96.994	1	0	

[SUBAREAS]


```

;;Subcatchment  N-Imperv  N-Perv  S-Imperv  S-Perv  PctZero  RouteTo  PctRouted
;;-----
S1              0.013   0.24   2.5      7.5     25       OUTLET

```

[INFILTRATION]

```

;;Subcatchment  Param1  Param2  Param3  Param4  Param5
;;-----
S1              75     0.5    4       7       0

```

[JUNCTIONS]

```

;;Name          Elevation  MaxDepth  InitDepth  SurDepth  Aponded
;;-----
J1              174.07   1.74    0        0        0

```

[OUTFALLS]

```

;;Name          Elevation  Type      Stage Data      Gated  Route To
;;-----
6R3879         174.05   TIMESERIES TW_5y4h_NorthNeighbourhood NO

```

[STORAGE]

```

;;Name          Elev.     MaxDepth  InitDepth  Shape      Curve Name/Params      N/A  Fevap  Psi  Ksat  IMD
;;-----
SU1            174.1    1.7      0          TABULAR   pipe_storage           0    0

```

[CONDUITS]

```

;;Name          From Node  To Node      Length  Roughness  InOffset  OutOffset  InitFlow  MaxFlow
;;-----
C1_2           J1         6R3879      14.951  0.013     0         0         0         0

```

[ORIFICES]

```

;;Name          From Node  To Node      Type      Offset  Qcoeff  Gated  CloseTime
;;-----
C1_1           SU1        J1           SIDE     0       0.63   NO     0

```

[XSECTIONS]

```

;;Link          Shape      Geom1      Geom2      Geom3      Geom4      Barrels  Culvert
;;-----
C1_2           CIRCULAR  0.525     0          0          0          1
C1_1           CIRCULAR  0.48      0          0          0

```

[LOSSES]

```

;;Link          Kentry  Kexit  Kavg  Flap Gate  Seepage
;;-----
C1_2           0.5    0.5   0     YES        0

```

[CURVES]

```

;;Name          Type      X-Value  Y-Value
;;-----
1              Storage  0        0.1
1              Storage  1        0.1
1              Storage  1.01    0.1
1              Storage  1.4     0.1
1              Storage  1.401   0.1
1              Storage  1.7     8400
pipe_storage   Storage  0        800
pipe_storage   Storage  0.675   800
pipe_storage   Storage  0.676   0.7

```

pipe_storage		1.4	0.7
pipe_storage		1.7	8400
pipe_storage_2	Storage	0	800
pipe_storage_2		1	800
pipe_storage_2		1.01	0.7
pipe_storage_2		1.4	0.7
pipe_storage_2		1.7	8400

[TIMESERIES]

;;Name	Date	Time	Value
100y24h2hDistribution		0:00	0
100y24h2hDistribution		2:00	1.08
100y24h2hDistribution		4:00	1.62
100y24h2hDistribution		6:00	1.62
100y24h2hDistribution		8:00	2.16
100y24h2hDistribution		10:00	3.24
100y24h2hDistribution		12:00	25.92
100y24h2hDistribution		14:00	8.64
100y24h2hDistribution		16:00	3.24
100y24h2hDistribution		18:00	2.16
100y24h2hDistribution		20:00	1.62
100y24h2hDistribution		22:00	1.62
100y24h2hDistribution		24:00	1.08
100y4h15mDistribution		0:00	3.95
100y4h15mDistribution		0:15	4.87
100y4h15mDistribution		0:30	6.36
100y4h15mDistribution		0:45	9.19
100y4h15mDistribution		1:00	16.45
100y4h15mDistribution		1:15	46.45
100y4h15mDistribution		1:30	143.67
100y4h15mDistribution		1:45	32.45
100y4h15mDistribution		2:00	17.25
100y4h15mDistribution		2:15	11.53
100y4h15mDistribution		2:30	8.62
100y4h15mDistribution		2:45	6.87
100y4h15mDistribution		3:00	5.71
100y4h15mDistribution		3:15	4.89
100y4h15mDistribution		3:30	4.28
100y4h15mDistribution		3:45	3.81
100y4h15mDistribution		4:00	0
5y4h15mDistribution		0:00	2.58
5y4h15mDistribution		0:15	3.13
5y4h15mDistribution		0:30	4.02
5y4h15mDistribution		0:45	5.66
5y4h15mDistribution		1:00	9.76
5y4h15mDistribution		1:15	26.72
5y4h15mDistribution		1:30	88.4
5y4h15mDistribution		1:45	18.73
5y4h15mDistribution		2:00	10.21
5y4h15mDistribution		2:15	6.99
5y4h15mDistribution		2:30	5.33
5y4h15mDistribution		2:45	4.31
5y4h15mDistribution		3:00	3.64

5y4h15mDistribution	3:15	3.15
5y4h15mDistribution	3:30	2.78
5y4h15mDistribution	3:45	2.49
5y4h15mDistribution	4:00	0

5y4h-6R3879	10:30:00	171.937119
5y4h-6R3879	10:35:00	171.937286
5y4h-6R3879	10:40:00	171.937622
5y4h-6R3879	10:45:00	171.937454
5y4h-6R3879	10:50:00	171.937805
5y4h-6R3879	10:55:00	171.938599
5y4h-6R3879	11:00:00	171.939102
5y4h-6R3879	11:05:00	171.940491
5y4h-6R3879	11:10:00	171.942795
5y4h-6R3879	11:15:00	171.943497
5y4h-6R3879	11:20:00	171.94632
5y4h-6R3879	11:25:00	171.949738
5y4h-6R3879	11:30:00	171.951202
5y4h-6R3879	11:35:00	171.955322
5y4h-6R3879	11:40:00	171.960815
5y4h-6R3879	11:45:00	171.963409
5y4h-6R3879	11:50:00	171.977341
5y4h-6R3879	11:55:00	171.989105
5y4h-6R3879	12:00:00	171.999557
5y4h-6R3879	12:05:00	172.055542
5y4h-6R3879	12:10:00	172.103683
5y4h-6R3879	12:15:00	172.158936
5y4h-6R3879	12:20:00	172.175262
5y4h-6R3879	12:25:00	172.189316
5y4h-6R3879	12:30:00	172.217773
5y4h-6R3879	12:35:00	172.231323
5y4h-6R3879	12:40:00	172.247726
5y4h-6R3879	12:45:00	172.267227
5y4h-6R3879	12:50:00	172.274887
5y4h-6R3879	12:55:00	172.283371
5y4h-6R3879	13:00:00	172.293091
5y4h-6R3879	13:05:00	172.298187
5y4h-6R3879	13:10:00	172.304413
5y4h-6R3879	13:15:00	172.312531
5y4h-6R3879	13:20:00	172.315155
5y4h-6R3879	13:25:00	172.31897
5y4h-6R3879	13:30:00	172.323013
5y4h-6R3879	13:35:00	172.325638
5y4h-6R3879	13:40:00	172.328934
5y4h-6R3879	13:45:00	172.332184
5y4h-6R3879	13:50:00	172.335968
5y4h-6R3879	13:55:00	172.33699
5y4h-6R3879	14:00:00	172.339127
5y4h-6R3879	14:05:00	172.341232
5y4h-6R3879	14:10:00	172.342987
5y4h-6R3879	14:15:00	172.345001
5y4h-6R3879	14:20:00	172.345612
5y4h-6R3879	14:25:00	172.347519
5y4h-6R3879	14:30:00	172.349152
5y4h-6R3879	14:35:00	172.349899
5y4h-6R3879	14:40:00	172.350784
5y4h-6R3879	14:45:00	172.351776

5y4h-6R3879	14:50:00	172.352249
5y4h-6R3879	14:55:00	172.353012
5y4h-6R3879	15:00:00	172.351776
5y4h-6R3879	15:05:00	172.35202
5y4h-6R3879	15:10:00	172.351929
5y4h-6R3879	15:15:00	172.351501
5y4h-6R3879	15:20:00	172.350922
5y4h-6R3879	15:25:00	172.350449
5y4h-6R3879	15:30:00	172.349945
5y4h-6R3879	15:35:00	172.349289
5y4h-6R3879	15:40:00	172.348587
5y4h-6R3879	15:45:00	172.347916
5y4h-6R3879	15:50:00	172.347244
5y4h-6R3879	15:55:00	172.346497
5y4h-6R3879	16:00:00	172.345734

TW_100y24h	0:00:00	171.977448
TW_100y24h	0:05:00	171.977448
TW_100y24h	0:10:00	171.977524
TW_100y24h	0:15:00	171.977448
TW_100y24h	0:20:00	171.977417
TW_100y24h	0:25:00	171.97757
TW_100y24h	0:30:00	171.977737
TW_100y24h	0:35:00	171.977951
TW_100y24h	0:40:00	171.978317
TW_100y24h	0:45:00	171.978729
TW_100y24h	0:50:00	171.979172
TW_100y24h	0:55:00	171.979691
TW_100y24h	1:00:00	171.980255
TW_100y24h	1:05:00	171.98082
TW_100y24h	1:10:00	171.98143
TW_100y24h	1:15:00	171.98204
TW_100y24h	1:20:00	171.982666
TW_100y24h	1:25:00	171.983948
TW_100y24h	1:30:00	171.984024
TW_100y24h	1:35:00	171.984467
TW_100y24h	1:40:00	171.985565
TW_100y24h	1:45:00	171.986038
TW_100y24h	1:50:00	171.986511
TW_100y24h	1:55:00	171.987427
TW_100y24h	2:00:00	171.988098
TW_100y24h	2:05:00	171.988754
TW_100y24h	2:10:00	171.989578
TW_100y24h	2:15:00	171.99028
TW_100y24h	2:20:00	171.991669
TW_100y24h	2:25:00	171.992065
TW_100y24h	2:30:00	171.992447
TW_100y24h	2:35:00	171.994049
TW_100y24h	2:40:00	171.995117
TW_100y24h	2:45:00	171.995804
TW_100y24h	2:50:00	171.99707
TW_100y24h	2:55:00	171.998245
TW_100y24h	3:00:00	171.99913
TW_100y24h	3:05:00	172.000015
TW_100y24h	3:10:00	172.000854
TW_100y24h	3:15:00	172.002518
TW_100y24h	3:20:00	172.003784

TW_100y24h	3:25:00	172.004562
TW_100y24h	3:30:00	172.005798
TW_100y24h	3:35:00	172.007034
TW_100y24h	3:40:00	172.007996
TW_100y24h	3:45:00	172.008865
TW_100y24h	3:50:00	172.009735
TW_100y24h	3:55:00	172.011337
TW_100y24h	4:00:00	172.012817
TW_100y24h	4:05:00	172.013535
TW_100y24h	4:10:00	172.014664
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TW_100y24h	4:25:00	172.018616
TW_100y24h	4:30:00	172.019089
TW_100y24h	4:35:00	172.020248
TW_100y24h	4:40:00	172.02179
TW_100y24h	4:45:00	172.022583
TW_100y24h	4:50:00	172.02359
TW_100y24h	4:55:00	172.024933
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TW_100y24h	5:30:00	172.03244
TW_100y24h	5:35:00	172.033813
TW_100y24h	5:40:00	172.034927
TW_100y24h	5:45:00	172.035858
TW_100y24h	5:50:00	172.037018
TW_100y24h	5:55:00	172.037796
TW_100y24h	6:00:00	172.038727
TW_100y24h	6:05:00	172.040375
TW_100y24h	6:10:00	172.04184
TW_100y24h	6:15:00	172.042587
TW_100y24h	6:20:00	172.043869
TW_100y24h	6:25:00	172.04538
TW_100y24h	6:30:00	172.046173
TW_100y24h	6:35:00	172.047394
TW_100y24h	6:40:00	172.049362
TW_100y24h	6:45:00	172.05101
TW_100y24h	6:50:00	172.052078
TW_100y24h	6:55:00	172.053543
TW_100y24h	7:00:00	172.055008
TW_100y24h	7:05:00	172.056015
TW_100y24h	7:10:00	172.057755
TW_100y24h	7:15:00	172.059647
TW_100y24h	7:20:00	172.06073
TW_100y24h	7:25:00	172.062057
TW_100y24h	7:30:00	172.064285
TW_100y24h	7:35:00	172.064896
TW_100y24h	7:40:00	172.066284
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TW_100y24h	7:50:00	172.069351
TW_100y24h	7:55:00	172.070572
TW_100y24h	8:00:00	172.073135
TW_100y24h	8:05:00	172.073914

TW_100y24h	8:10:00	172.075134
TW_100y24h	8:15:00	172.076965
TW_100y24h	8:20:00	172.078644
TW_100y24h	8:25:00	172.08046
TW_100y24h	8:30:00	172.082047
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TW_100y24h	8:40:00	172.086609
TW_100y24h	8:45:00	172.088959
TW_100y24h	8:50:00	172.090302
TW_100y24h	8:55:00	172.092651
TW_100y24h	9:00:00	172.095062
TW_100y24h	9:05:00	172.097809
TW_100y24h	9:10:00	172.098969
TW_100y24h	9:15:00	172.10112
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TW_100y24h	9:55:00	172.117676
TW_100y24h	10:00:00	172.120163
TW_100y24h	10:05:00	172.13147
TW_100y24h	10:10:00	172.136948
TW_100y24h	10:15:00	172.141449
TW_100y24h	10:20:00	172.159821
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TW_100y24h	10:45:00	172.2435
TW_100y24h	10:50:00	172.260025
TW_100y24h	10:55:00	172.276245
TW_100y24h	11:00:00	172.29689
TW_100y24h	11:05:00	172.313477
TW_100y24h	11:10:00	172.328705
TW_100y24h	11:15:00	172.348785
TW_100y24h	11:20:00	172.364319
TW_100y24h	11:25:00	172.380966
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TW_100y24h	11:35:00	172.417938
TW_100y24h	11:40:00	172.43364
TW_100y24h	11:45:00	172.454437
TW_100y24h	11:50:00	172.469467
TW_100y24h	11:55:00	172.490005
TW_100y24h	12:00:00	172.507187
TW_100y24h	12:05:00	172.516296
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TW_100y24h	12:30:00	172.566635
TW_100y24h	12:35:00	172.573837
TW_100y24h	12:40:00	172.579285
TW_100y24h	12:45:00	172.584915
TW_100y24h	12:50:00	172.591782

TW_100y24h	12:55:00	172.597778
TW_100y24h	13:00:00	172.603683
TW_100y24h	13:05:00	172.609573
TW_100y24h	13:10:00	172.617432
TW_100y24h	13:15:00	172.620926
TW_100y24h	13:20:00	172.628357
TW_100y24h	13:25:00	172.632309
TW_100y24h	13:30:00	172.638855
TW_100y24h	13:35:00	172.644012
TW_100y24h	13:40:00	172.649323
TW_100y24h	13:45:00	172.655685
TW_100y24h	13:50:00	172.661224
TW_100y24h	13:55:00	172.668976
TW_100y24h	14:00:00	172.672348
TW_100y24h	14:05:00	172.678284
TW_100y24h	14:10:00	172.680954
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TW_100y24h	14:20:00	172.688766
TW_100y24h	14:25:00	172.691803
TW_100y24h	14:30:00	172.692841
TW_100y24h	14:35:00	172.694992
TW_100y24h	14:40:00	172.697037
TW_100y24h	14:45:00	172.699585
TW_100y24h	14:50:00	172.700302
TW_100y24h	14:55:00	172.702408
TW_100y24h	15:00:00	172.704041
TW_100y24h	15:05:00	172.706329
TW_100y24h	15:10:00	172.707047
TW_100y24h	15:15:00	172.708908
TW_100y24h	15:20:00	172.71051
TW_100y24h	15:25:00	172.712082
TW_100y24h	15:30:00	172.713303
TW_100y24h	15:35:00	172.715012
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TW_100y24h	15:50:00	172.719513
TW_100y24h	15:55:00	172.720993
TW_100y24h	16:00:00	172.722565
TW_100y24h	16:05:00	172.723618
TW_100y24h	16:10:00	172.725067
TW_100y24h	16:15:00	172.726227
TW_100y24h	16:20:00	172.727432
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TW_100y24h	16:30:00	172.72905
TW_100y24h	16:35:00	172.729752
TW_100y24h	16:40:00	172.730331
TW_100y24h	16:45:00	172.731186
TW_100y24h	16:50:00	172.732025
TW_100y24h	16:55:00	172.732483
TW_100y24h	17:00:00	172.733154
TW_100y24h	17:05:00	172.733765
TW_100y24h	17:10:00	172.734528
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TW_100y24h	17:30:00	172.736862
TW_100y24h	17:35:00	172.737305

TW_100y24h	17:40:00	172.737778
TW_100y24h	17:45:00	172.738312
TW_100y24h	17:50:00	172.739136
TW_100y24h	17:55:00	172.739227
TW_100y24h	18:00:00	172.740295
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TW_100y24h	19:15:00	172.7435
TW_100y24h	19:20:00	172.743591
TW_100y24h	19:25:00	172.743668
TW_100y24h	19:30:00	172.744141
TW_100y24h	19:35:00	172.743729
TW_100y24h	19:40:00	172.744019
TW_100y24h	19:45:00	172.744049
TW_100y24h	19:50:00	172.744186
TW_100y24h	19:55:00	172.744095
TW_100y24h	20:00:00	172.744202
TW_100y24h	20:05:00	172.744278
TW_100y24h	20:10:00	172.745148
TW_100y24h	20:15:00	172.744034
TW_100y24h	20:20:00	172.744431
TW_100y24h	20:25:00	172.744537
TW_100y24h	20:30:00	172.744629
TW_100y24h	20:35:00	172.744446
TW_100y24h	20:40:00	172.744492
TW_100y24h	20:45:00	172.744614
TW_100y24h	20:50:00	172.744553
TW_100y24h	20:55:00	172.744415
TW_100y24h	21:00:00	172.744583
TW_100y24h	21:05:00	172.74472
TW_100y24h	21:10:00	172.744553
TW_100y24h	21:15:00	172.744644
TW_100y24h	21:20:00	172.744522
TW_100y24h	21:25:00	172.744675
TW_100y24h	21:30:00	172.74437
TW_100y24h	21:35:00	172.744522
TW_100y24h	21:40:00	172.744476
TW_100y24h	21:45:00	172.744598
TW_100y24h	21:50:00	172.744171
TW_100y24h	21:55:00	172.744522
TW_100y24h	22:00:00	172.74437
TW_100y24h	22:05:00	172.744324
TW_100y24h	22:10:00	172.744034
TW_100y24h	22:15:00	172.743805
TW_100y24h	22:20:00	172.743713

TW_100y24h	22:25:00	172.743637
TW_100y24h	22:30:00	172.742966
TW_100y24h	22:35:00	172.743011
TW_100y24h	22:40:00	172.742477
TW_100y24h	22:45:00	172.742142
TW_100y24h	22:50:00	172.741714
TW_100y24h	22:55:00	172.741318
TW_100y24h	23:00:00	172.740891
TW_100y24h	23:05:00	172.740417
TW_100y24h	23:10:00	172.740112
TW_100y24h	23:15:00	172.740051
TW_100y24h	23:20:00	172.738983
TW_100y24h	23:25:00	172.738708
TW_100y24h	23:30:00	172.738266
TW_100y24h	23:35:00	172.737946
TW_100y24h	23:40:00	172.737289
TW_100y24h	23:45:00	172.736847
TW_100y24h	23:50:00	172.736374
TW_100y24h	23:55:00	172.73584
TW_100y24h	24:00:00	172.735413

TW_100y24h_Northneighbourhood	4/11/2022	0:00	172.1956
TW_100y24h_Northneighbourhood	4/11/2022	0:02	172.1925
TW_100y24h_Northneighbourhood	4/11/2022	0:04	172.2101
TW_100y24h_Northneighbourhood	4/11/2022	0:06	172.1977
TW_100y24h_Northneighbourhood	4/11/2022	0:08	172.2034
TW_100y24h_Northneighbourhood	4/11/2022	0:10	172.1968
TW_100y24h_Northneighbourhood	4/11/2022	0:12	172.1996
TW_100y24h_Northneighbourhood	4/11/2022	0:14	172.2007
TW_100y24h_Northneighbourhood	4/11/2022	0:16	172.1944
TW_100y24h_Northneighbourhood	4/11/2022	0:18	172.1977
TW_100y24h_Northneighbourhood	4/11/2022	0:20	172.1961

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Too many data points (2160 in total).

TW_100Y4h	0:00:00	171.937119
TW_100Y4h	0:05:00	171.937424
TW_100Y4h	0:10:00	171.938034
TW_100Y4h	0:15:00	171.937683
TW_100Y4h	0:20:00	171.938492
TW_100Y4h	0:25:00	171.940002
TW_100Y4h	0:30:00	171.94194
TW_100Y4h	0:35:00	171.943878
TW_100Y4h	0:40:00	171.946487
TW_100Y4h	0:45:00	171.949646
TW_100Y4h	0:50:00	171.9534
TW_100Y4h	0:55:00	171.959442
TW_100Y4h	1:00:00	171.962891
TW_100Y4h	1:05:00	171.97084
TW_100Y4h	1:10:00	171.978561
TW_100Y4h	1:15:00	171.98642
TW_100Y4h	1:20:00	172.012711
TW_100Y4h	1:25:00	172.034943
TW_100Y4h	1:30:00	172.058777
TW_100Y4h	1:35:00	172.154663
TW_100Y4h	1:40:00	172.251862
TW_100Y4h	1:45:00	172.347977

TW_100Y4h	1:50:00	172.358475	
TW_100Y4h	1:55:00	172.36882	
TW_100Y4h	2:00:00	172.403534	
TW_100Y4h	2:05:00	172.428757	
TW_100Y4h	2:10:00	172.456833	
TW_100Y4h	2:15:00	172.485352	
TW_100Y4h	2:20:00	172.506775	
TW_100Y4h	2:25:00	172.528168	
TW_100Y4h	2:30:00	172.548935	
TW_100Y4h	2:35:00	172.564743	
TW_100Y4h	2:40:00	172.579163	
TW_100Y4h	2:45:00	172.592468	
TW_100Y4h	2:50:00	172.602844	
TW_100Y4h	2:55:00	172.616302	
TW_100Y4h	3:00:00	172.624084	
TW_100Y4h	3:05:00	172.632553	
TW_100Y4h	3:10:00	172.641678	
TW_100Y4h	3:15:00	172.649323	
TW_100Y4h	3:20:00	172.656235	
TW_100Y4h	3:25:00	172.662628	
TW_100Y4h	3:30:00	172.668274	
TW_100Y4h	3:35:00	172.673706	
TW_100Y4h	3:40:00	172.678406	
TW_100Y4h	3:45:00	172.683319	
TW_100Y4h	3:50:00	172.688583	
TW_100Y4h	3:55:00	172.691223	
TW_100Y4h	4:00:00	172.695435	
TW_100Y4h	4:05:00	172.698303	
TW_100Y4h	4:10:00	172.701523	
TW_100Y4h	4:15:00	172.703033	
TW_100Y4h	4:20:00	172.7052	
TW_100Y4h	4:25:00	172.706787	
TW_100Y4h	4:30:00	172.707245	
TW_100Y4h	4:35:00	172.707733	
TW_100Y4h	4:40:00	172.708191	
TW_100Y4h	4:45:00	172.708664	
TW_100Y4h	4:50:00	172.708618	
TW_100Y4h	4:55:00	172.708664	
TW_100Y4h	5:00:00	172.708466	
TW_100Y4h	5:05:00	172.708313	
TW_100Y4h	5:10:00	172.708069	
TW_100Y4h	5:15:00	172.707794	
TW_100Y4h	5:20:00	172.707352	
TW_100Y4h	5:25:00	172.706894	
TW_100Y4h	5:30:00	172.706467	
TW_100y4h_NorthNeighbourhood	4/11/2022	0:00	172.1956
TW_100y4h_NorthNeighbourhood	4/11/2022	0:02	172.1925
TW_100y4h_NorthNeighbourhood	4/11/2022	0:04	172.2101
TW_100y4h_NorthNeighbourhood	4/11/2022	0:06	172.1977
TW_100y4h_NorthNeighbourhood	4/11/2022	0:08	172.2034
TW_100y4h_NorthNeighbourhood	4/11/2022	0:10	172.1968
TW_100y4h_NorthNeighbourhood	4/11/2022	0:12	172.1996
TW_100y4h_NorthNeighbourhood	4/11/2022	0:14	172.2007
TW_100y4h_NorthNeighbourhood	4/11/2022	0:16	172.1944
TW_100y4h_NorthNeighbourhood	4/11/2022	0:18	172.1977
TW_100y4h_NorthNeighbourhood	4/11/2022	0:20	172.1961

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Too many data points (1080 in total).

TW_5y4h_NorthNeighbourhood	4/11/2022	0:00	172.1956
TW_5y4h_NorthNeighbourhood	4/11/2022	0:02	172.1925
TW_5y4h_NorthNeighbourhood	4/11/2022	0:04	172.2101
TW_5y4h_NorthNeighbourhood	4/11/2022	0:06	172.1977
TW_5y4h_NorthNeighbourhood	4/11/2022	0:08	172.2034
TW_5y4h_NorthNeighbourhood	4/11/2022	0:10	172.1968
TW_5y4h_NorthNeighbourhood	4/11/2022	0:12	172.1996
TW_5y4h_NorthNeighbourhood	4/11/2022	0:14	172.2007
TW_5y4h_NorthNeighbourhood	4/11/2022	0:16	172.1944
TW_5y4h_NorthNeighbourhood	4/11/2022	0:18	172.1977
TW_5y4h_NorthNeighbourhood	4/11/2022	0:20	172.1961

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Too many data points (1080 in total).

TW_UST_Northneighbourhood	4/11/2022	0:00	172.1956
TW_UST_Northneighbourhood	4/11/2022	0:02	172.1925
TW_UST_Northneighbourhood	4/11/2022	0:04	172.2101
TW_UST_Northneighbourhood	4/11/2022	0:06	172.1977
TW_UST_Northneighbourhood	4/11/2022	0:08	172.2034
TW_UST_Northneighbourhood	4/11/2022	0:10	172.1968
TW_UST_Northneighbourhood	4/11/2022	0:12	172.1996
TW_UST_Northneighbourhood	4/11/2022	0:14	172.2007
TW_UST_Northneighbourhood	4/11/2022	0:16	172.1944
TW_UST_Northneighbourhood	4/11/2022	0:18	172.1977
TW_UST_Northneighbourhood	4/11/2022	0:20	172.1961

.....

Too many data points (2160 in total).

UST	0:00	2.41
UST	0:15	2.43
UST	0:30	2.45
UST	0:45	2.46
UST	1:00	2.48
UST	1:15	2.51
UST	1:30	2.53
UST	1:45	2.55
UST	2:00	2.58
UST	2:15	2.61
UST	2:30	2.64
UST	2:45	2.67
UST	3:00	2.71
UST	3:15	2.74
UST	3:30	2.79
UST	3:45	2.83
UST	4:00	2.88
UST	4:15	2.94
UST	4:30	3
UST	4:45	3.07
UST	5:00	3.15
UST	5:15	3.23
UST	5:30	3.33
UST	5:45	3.45
UST	6:00	3.59
UST	6:15	3.75

UST	6:30	3.94
UST	6:45	4.18
UST	7:00	4.49
UST	7:15	4.89
UST	7:30	5.43
UST	7:45	6.2
UST	8:00	7.41
UST	8:15	9.56
UST	8:30	14.29
UST	8:45	32.01
UST	9:00	145.13
UST	9:15	48.51
UST	9:30	23.13
UST	9:45	15.08
UST	10:00	11.35
UST	10:15	9.23
UST	10:30	7.88
UST	10:45	6.94
UST	11:00	6.25
UST	11:15	5.73
UST	11:30	5.32
UST	11:45	4.99
UST	12:00	4.72
UST	12:15	4.49
UST	12:30	4.29
UST	12:45	4.12
UST	13:00	3.98
UST	13:15	3.85
UST	13:30	3.74
UST	13:45	3.63
UST	14:00	3.54
UST	14:15	3.46
UST	14:30	3.39
UST	14:45	3.32
UST	15:00	3.26
UST	15:15	3.2
UST	15:30	3.15
UST	15:45	3.1
UST	16:00	3.05
UST	16:15	3.01
UST	16:30	2.97
UST	16:45	2.93
UST	17:00	2.9
UST	17:15	2.87
UST	17:30	2.84
UST	17:45	2.81
UST	18:00	2.78
UST	18:15	2.76
UST	18:30	2.73
UST	18:45	2.71
UST	19:00	2.69
UST	19:15	2.67
UST	19:30	2.65
UST	19:45	2.63
UST	20:00	2.61
UST	20:15	2.59
UST	20:30	2.57

UST	20:45	2.56
UST	21:00	2.54
UST	21:15	2.53
UST	21:30	2.51
UST	21:45	2.5
UST	22:00	2.49
UST	22:15	2.47
UST	22:30	2.46
UST	22:45	2.45
UST	23:00	2.44
UST	23:15	2.43
UST	23:30	2.42
UST	23:45	2.41

WaterQualityTest	00:00	1.78
WaterQualityTest	00:15	2.13
WaterQualityTest	00:30	2.7
WaterQualityTest	00:45	3.72
WaterQualityTest	01:00	6.21
WaterQualityTest	01:15	16.41
WaterQualityTest	01:30	57.83
WaterQualityTest	01:45	11.58
WaterQualityTest	02:00	6.48
WaterQualityTest	02:15	4.53
WaterQualityTest	02:30	3.51
WaterQualityTest	02:45	2.88
WaterQualityTest	03:00	2.45
WaterQualityTest	03:15	2.14
WaterQualityTest	03:30	1.91
WaterQualityTest	03:45	1.72
WaterQualityTest	04:00	0

```
[REPORT]
;;Reporting Options
INPUT      YES
CONTROLS   NO
SUBCATCHMENTS ALL
NODES ALL
LINKS ALL
```

```
[TAGS]
```

```
[MAP]
DIMENSIONS      341763.63845      4688380.22915      342012.07455      4688622.75385
UNITS           Meters
```

```
[COORDINATES]
;;Node          X-Coord          Y-Coord
;;-----
J1              341797.404          4688593.489
6R3879          341784.931          4688601.73
SU1             341810.01           4688585.16
```

```
[VERTICES]
;;Link          X-Coord          Y-Coord
;;-----
```

```
[POLYGONS]
```

```
;;Subcatchment X-Coord Y-Coord
;;-----
S1 341796.575 4688595.46
S1 341954.176 4688593.45
S1 341955.354 4688582.553
S1 341972.053 4688584.903
S1 342000.782 4688419.018
S1 341828.818 4688391.253
S1 341796.575 4688595.46
```

```
[SYMBOLS]
;;Gage X-Coord Y-Coord
;;-----
```

PCSWMM Output Report: 1:5 year 4 hour

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

Element Count

Number of rain gages 1
 Number of subcatchments ... 1
 Number of nodes 3
 Number of links 2
 Number of pollutants 0
 Number of land uses 0

Raingage Summary

Name	Data Source	Data Type	Recording Interval
Raingage1	5y4h15mDistribution	INTENSITY	15 min.

Subcatchment Summary

Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
S1	3.30	96.99	90.00	1.0000	Raingage1	SU1

Node Summary

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
J1	JUNCTION	174.07	1.74	0.0	
6R3879	OUTFALL	174.05	0.53	0.0	
SU1	STORAGE	174.10	1.70	0.0	

Link Summary

Name	From Node	To Node	Type	Length	%Slope	Roughness
C1_2	J1	6R3879	CONDUIT	15.0	0.1338	0.0130
C1_1	SU1	J1	ORIFICE			

Cross Section Summary

Full	Full	Hyd.	Max.	No. of	Full
------	------	------	------	--------	------

Conduit	Shape	Depth	Area	Rad.	Width	Barrels	Flow
C1_2	CIRCULAR	0.53	0.22	0.13	0.53	1	0.16

NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.

Analysis Options

Flow Units CMS

Process Models:

Rainfall/Runoff YES
RDII NO
Snowmelt NO
Groundwater NO
Flow Routing YES
Ponding Allowed NO
Water Quality NO

Infiltration Method HORTON

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 04/11/2022 00:00:00

Ending Date 04/12/2022 12:00:00

Antecedent Dry Days 0.0

Report Time Step 00:01:00

Wet Time Step 00:05:00

Dry Time Step 00:05:00

Routing Time Step 1.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.001500 m

	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm

Total Precipitation	0.163	49.475
Evaporation Loss	0.000	0.000
Infiltration Loss	0.010	2.889
Surface Runoff	0.149	45.068
Final Storage	0.006	1.698
Continuity Error (%)	-0.363	

	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr

Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.149	1.486
Groundwater Inflow	0.000	0.000


```

RDII Inflow ..... 0.000 0.000
External Inflow ..... 0.000 0.000
External Outflow ..... 0.149 1.486
Flooding Loss ..... 0.000 0.000
Evaporation Loss ..... 0.000 0.000
Exfiltration Loss ..... 0.000 0.000
Initial Stored Volume .... 0.000 0.000
Final Stored Volume ..... 0.000 0.001
Continuity Error (%) ..... -0.017

```

```

*****
Time-Step Critical Elements
*****
None

```

```

*****
Highest Flow Instability Indexes
*****
All links are stable.

```

```

*****
Routing Time Step Summary
*****
Minimum Time Step      : 0.50 sec
Average Time Step      : 1.00 sec
Maximum Time Step      : 1.00 sec
Percent in Steady State : 0.00
Average Iterations per Step : 2.00
Percent Not Converging  : 0.01
Time Step Frequencies  :
  1.000 - 0.871 sec    : 100.00 %
  0.871 - 0.758 sec    : 0.00 %
  0.758 - 0.660 sec    : 0.00 %
  0.660 - 0.574 sec    : 0.00 %
  0.574 - 0.500 sec    : 0.00 %

```

```

*****
Subcatchment Runoff Summary
*****

```

Subcatchment	Total Precip mm	Total Runon mm	Total Evap mm	Total Infil mm	Imperv Runoff mm	Perv Runoff mm	Total Runoff mm	Total Runoff 10 ⁶ ltr	Peak Runoff CMS	Runoff Coeff
S1	49.47	0.00	0.00	2.89	42.99	2.07	45.07	1.49	0.66	0.911

```

*****
Node Depth Summary
*****

```

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
J1	JUNCTION	0.05	0.81	174.88	0 01:49	0.77
6R3879	OUTFALL	0.03	0.43	174.48	0 01:50	0.43
SU1	STORAGE	0.05	1.40	175.50	0 01:50	1.40

Node Inflow Summary

Node	Type	Maximum Lateral Inflow CMS	Maximum Total Inflow CMS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 ltr	Total Inflow Volume 10^6 ltr	Flow Balance Error Percent
J1	JUNCTION	0.000	0.412	0 01:50	0	1.49	-0.014
6R3879	OUTFALL	0.000	0.412	0 01:50	0	1.49	0.000
SU1	STORAGE	0.665	0.665	0 01:45	1.49	1.49	-0.002

Node Surcharge Summary

Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Meters	Min. Depth Below Rim Meters
J1	JUNCTION	0.16	0.285	0.930

Node Flooding Summary

No nodes were flooded.

Storage Volume Summary

Storage Unit	Average Volume 1000 m3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m3	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow CMS
SU1	0.035	2	0	0	0.541	30	0 01:50	0.412

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CMS	Max Flow CMS	Total Volume 10^6 ltr
6R3879	75.58	0.015	0.412	1.486
System	75.58	0.015	0.412	1.486

 Link Flow Summary

Link	Type	Maximum Flow CMS	Time of Max Occurrence days hr:min	Maximum Veloc m/sec	Max/ Full Flow	Max/ Full Depth
C1_2	CONDUIT	0.412	0 01:50	1.99	2.62	0.91
C1_1	ORIFICE	0.412	0 01:50			1.00

 Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class									
		Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl		
C1_2	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00

 Conduit Surcharge Summary

Conduit	Hours Full			Hours Above Normal Flow	Hours Capacity Limited
	Both Ends	Upstream	Dnstream	Flow	Limited
C1_2	0.01	0.16	0.01	0.93	0.01

Analysis begun on: Thu Jun 30 09:27:17 2022
 Analysis ended on: Thu Jun 30 09:27:17 2022
 Total elapsed time: < 1 sec

PCSWMM Output Report: 1:100 year 4 hour

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

Element Count

Number of rain gages 1
 Number of subcatchments ... 1
 Number of nodes 3
 Number of links 2
 Number of pollutants 0
 Number of land uses 0

Raingage Summary

Name	Data Source	Data Type	Recording Interval
Raingage1	100y4h15mDistribution	INTENSITY	15 min.

Subcatchment Summary

Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
S1	3.30	96.99	90.00	1.0000	Raingage1	SU1

Node Summary

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
J1	JUNCTION	174.07	1.74	0.0	
6R3879	OUTFALL	174.05	0.53	0.0	
SU1	STORAGE	174.10	1.70	0.0	

Link Summary

Name	From Node	To Node	Type	Length	%Slope	Roughness
C1_2	J1	6R3879	CONDUIT	15.0	0.1338	0.0130
C1_1	SU1	J1	ORIFICE			

Cross Section Summary

Full	Full	Hyd.	Max.	No. of	Full
------	------	------	------	--------	------

Conduit	Shape	Depth	Area	Rad.	Width	Barrels	Flow
C1_2	CIRCULAR	0.53	0.22	0.13	0.53	1	0.16

NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.

Analysis Options

Flow Units CMS

Process Models:

Rainfall/Runoff YES
RDII NO
Snowmelt NO
Groundwater NO
Flow Routing YES
Ponding Allowed NO
Water Quality NO

Infiltration Method HORTON

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 04/11/2022 00:00:00

Ending Date 04/12/2022 12:00:00

Antecedent Dry Days 0.0

Report Time Step 00:01:00

Wet Time Step 00:05:00

Dry Time Step 00:05:00

Routing Time Step 1.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.001500 m

	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
Total Precipitation	0.269	81.587
Evaporation Loss	0.000	0.000
Infiltration Loss	0.010	2.908
Surface Runoff	0.255	77.317
Final Storage	0.006	1.698
Continuity Error (%)	-0.410	

	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.255	2.550
Groundwater Inflow	0.000	0.000

```

RDII Inflow ..... 0.000 0.000
External Inflow ..... 0.000 0.000
External Outflow ..... 0.253 2.531
Flooding Loss ..... 0.000 0.000
Evaporation Loss ..... 0.000 0.000
Exfiltration Loss ..... 0.000 0.000
Initial Stored Volume .... 0.000 0.000
Final Stored Volume ..... 0.000 0.001
Continuity Error (%) ..... 0.707

```

```

*****
Time-Step Critical Elements
*****
None

```

```

*****
Highest Flow Instability Indexes
*****
All links are stable.

```

```

*****
Routing Time Step Summary
*****
Minimum Time Step      : 0.50 sec
Average Time Step      : 1.00 sec
Maximum Time Step      : 1.00 sec
Percent in Steady State : 0.00
Average Iterations per Step : 2.00
Percent Not Converging  : 0.00
Time Step Frequencies :
  1.000 - 0.871 sec    : 100.00 %
  0.871 - 0.758 sec    : 0.00 %
  0.758 - 0.660 sec    : 0.00 %
  0.660 - 0.574 sec    : 0.00 %
  0.574 - 0.500 sec    : 0.00 %

```

```

*****
Subcatchment Runoff Summary
*****

```

Subcatchment	Total Precip mm	Total Runon mm	Total Evap mm	Total Infil mm	Imperv Runoff mm	Perv Runoff mm	Total Runoff mm	Total Runoff 10 ⁶ ltr	Peak Runoff CMS	Runoff Coeff
S1	81.59	0.00	0.00	2.91	72.02	5.30	77.32	2.55	1.19	0.948

```

*****
Node Depth Summary
*****

```

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
J1	JUNCTION	0.06	1.01	175.08	0 01:38	0.86
6R3879	OUTFALL	0.04	0.45	174.50	0 01:57	0.45
SU1	STORAGE	0.07	1.58	175.68	0 01:57	1.58

Node Inflow Summary

Node	Type	Maximum Lateral Inflow CMS	Maximum Total Inflow CMS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 ltr	Total Inflow Volume 10^6 ltr	Flow Balance Error Percent
J1	JUNCTION	0.000	0.446	0 01:57	0	2.53	0.002
6R3879	OUTFALL	0.000	0.446	0 01:57	0	2.53	0.000
SU1	STORAGE	1.188	1.188	0 01:45	2.55	2.55	0.711

Node Surcharge Summary

Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Meters	Min. Depth Below Rim Meters
J1	JUNCTION	0.91	0.483	0.732

Node Flooding Summary

No nodes were flooded.

Storage Volume Summary

Storage Unit	Average Volume 1000 m3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m3	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow CMS
SU1	0.050	3	0	0	0.984	55	0 01:57	0.446

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CMS	Max Flow CMS	Total Volume 10^6 ltr
6R3879	76.32	0.026	0.446	2.531
System	76.32	0.026	0.446	2.531

Link Flow Summary

Link	Type	Maximum Flow CMS	Time of Max Occurrence days hr:min	Maximum Veloc m/sec	Max/ Full Flow	Max/ Full Depth
C1_2	CONDUIT	0.446	0 01:57	2.13	2.83	0.93
C1_1	ORIFICE	0.446	0 01:57			1.00

Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class								
		Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl	
C1_2	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00

Conduit Surcharge Summary

Conduit	Hours Full			Hours Above Normal Flow	Hours Capacity Limited
	Both Ends	Upstream	Dnstream	Full Flow	Limited
C1_2	0.01	0.91	0.01	1.41	0.01

Analysis begun on: Thu Jun 30 09:26:52 2022
 Analysis ended on: Thu Jun 30 09:26:53 2022
 Total elapsed time: 00:00:01

PCSWMM Output Report: 1:100 year 24 hour

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

Element Count

Number of rain gages 1
 Number of subcatchments ... 1
 Number of nodes 3
 Number of links 2
 Number of pollutants 0
 Number of land uses 0

Raingage Summary

Name	Data Source	Data Type	Recording Interval
Raingage1	100y24h2hDistribution	INTENSITY	120 min.

Subcatchment Summary

Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
S1	3.30	96.99	90.00	1.0000	Raingage1	SU1

Node Summary

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
J1	JUNCTION	174.07	1.74	0.0	
6R3879	OUTFALL	174.05	0.53	0.0	
SU1	STORAGE	174.10	1.70	0.0	

Link Summary

Name	From Node	To Node	Type	Length	%Slope	Roughness
C1_2	J1	6R3879	CONDUIT	15.0	0.1338	0.0130
C1_1	SU1	J1	ORIFICE			

Cross Section Summary

Full	Full	Hyd.	Max.	No. of	Full
------	------	------	------	--------	------

Conduit	Shape	Depth	Area	Rad.	Width	Barrels	Flow
C1_2	CIRCULAR	0.53	0.22	0.13	0.53	1	0.16

NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.

Analysis Options

Flow Units CMS

Process Models:

Rainfall/Runoff YES
RDII NO
Snowmelt NO
Groundwater NO
Flow Routing YES
Ponding Allowed NO
Water Quality NO

Infiltration Method HORTON

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 04/11/2022 00:00:00

Ending Date 04/12/2022 12:00:00

Antecedent Dry Days 0.0

Report Time Step 00:01:00

Wet Time Step 00:05:00

Dry Time Step 00:05:00

Routing Time Step 2.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.001500 m

	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm

Total Precipitation	0.356	108.000
Evaporation Loss	0.000	0.000
Infiltration Loss	0.010	3.121
Surface Runoff	0.339	102.841
Final Storage	0.007	2.078
Continuity Error (%)	-0.036	

	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr

Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.339	3.392
Groundwater Inflow	0.000	0.000

```

RDII Inflow ..... 0.000 0.000
External Inflow ..... 0.000 0.000
External Outflow ..... 0.339 3.387
Flooding Loss ..... 0.000 0.000
Evaporation Loss ..... 0.000 0.000
Exfiltration Loss ..... 0.000 0.000
Initial Stored Volume .... 0.000 0.000
Final Stored Volume ..... 0.000 0.004
Continuity Error (%) ..... 0.000

```

```

*****
Time-Step Critical Elements
*****
None

```

```

*****
Highest Flow Instability Indexes
*****
All links are stable.

```

```

*****
Routing Time Step Summary
*****
Minimum Time Step      : 1.50 sec
Average Time Step      : 2.00 sec
Maximum Time Step      : 2.00 sec
Percent in Steady State : 0.00
Average Iterations per Step : 2.00
Percent Not Converging  : 0.00
Time Step Frequencies :
  2.000 - 1.516 sec    : 100.00 %
  1.516 - 1.149 sec    : 0.00 %
  1.149 - 0.871 sec    : 0.00 %
  0.871 - 0.660 sec    : 0.00 %
  0.660 - 0.500 sec    : 0.00 %

```

```

*****
Subcatchment Runoff Summary
*****

```

Subcatchment	Total Precip mm	Total Runon mm	Total Evap mm	Total Infil mm	Imperv Runoff mm	Perv Runoff mm	Total Runoff mm	Total Runoff 10 ⁶ ltr	Peak Runoff CMS	Runoff Coeff
S1	108.00	0.00	0.00	3.12	95.50	7.34	102.84	3.39	0.24	0.952

```

*****
Node Depth Summary
*****

```

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
J1	JUNCTION	0.11	0.47	174.54	0 14:01	0.47
6R3879	OUTFALL	0.08	0.32	174.37	0 14:01	0.32
SU1	STORAGE	0.11	0.64	174.74	0 14:01	0.64

Node Inflow Summary

Node	Type	Maximum Lateral Inflow CMS	Maximum Total Inflow CMS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 ltr	Total Inflow Volume 10^6 ltr	Flow Balance Error Percent
J1	JUNCTION	0.000	0.224	0 14:01	0	3.39	0.001
6R3879	OUTFALL	0.000	0.224	0 14:01	0	3.39	0.000
SU1	STORAGE	0.237	0.237	0 14:00	3.39	3.39	0.000

Node Surcharge Summary

No nodes were surcharged.

Node Flooding Summary

No nodes were flooded.

Storage Volume Summary

Storage Unit	Average Volume 1000 m3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m3	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow CMS
SU1	0.090	5	0	0	0.509	28	0 14:01	0.224

Outfall Loading Summary

Flow Freq	Avg Flow	Max Flow	Total Volume
-----------	----------	----------	--------------

Outfall Node	Pcnt	CMS	CMS	10^6 ltr
6R3879	92.32	0.028	0.224	3.387
System	92.32	0.028	0.224	3.387

Link Flow Summary

Link	Type	Maximum Flow CMS	Time of Max Occurrence days hr:min	Maximum Veloc m/sec	Max/ Full Flow	Max/ Full Depth
C1_2	CONDUIT	0.224	0 14:01	1.28	1.42	0.75
C1_1	ORIFICE	0.224	0 14:01			1.00

Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class								
		Up Dry	Down Dry	Sub Dry	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl	
C1_2	1.00	0.06	0.00	0.00	0.94	0.00	0.00	0.00	0.00	0.00

Conduit Surcharge Summary

Conduit	Hours Full			Hours	Hours
	Both Ends	Upstream	Dnstream	Above Full Normal Flow	Capacity Limited
C1_2	0.01	0.01	0.01	1.75	0.01

Analysis begun on: Thu Jun 30 09:27:45 2022
Analysis ended on: Thu Jun 30 09:27:45 2022
Total elapsed time: < 1 sec

PCSWMM Output Report: Urban Stress Test

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.1 (Build 5.1.015)

Element Count

Number of rain gages 1
 Number of subcatchments ... 1
 Number of nodes 3
 Number of links 2
 Number of pollutants 0
 Number of land uses 0

Raingage Summary

Name	Data Source	Data Type	Recording Interval
Raingage1	UST	INTENSITY	15 min.

Subcatchment Summary

Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
S1	3.30	96.99	90.00	1.0000	Raingage1	SU1

Node Summary

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
J1	JUNCTION	174.07	1.74	0.0	
6R3879	OUTFALL	174.05	0.53	0.0	
SU1	STORAGE	174.10	1.70	0.0	

Link Summary

Name	From Node	To Node	Type	Length	%Slope	Roughness
C1_2	J1	6R3879	CONDUIT	15.0	0.1338	0.0130
C1_1	SU1	J1	ORIFICE			

Cross Section Summary

Full	Full	Hyd.	Max.	No. of	Full
------	------	------	------	--------	------

Conduit	Shape	Depth	Area	Rad.	Width	Barrels	Flow
C1_2	CIRCULAR	0.53	0.22	0.13	0.53	1	0.16

NOTE: The summary statistics displayed in this report are based on results found at every computational time step, not just on results from each reporting time step.

Analysis Options

Flow Units CMS

Process Models:

Rainfall/Runoff YES
RDII NO
Snowmelt NO
Groundwater NO
Flow Routing YES
Ponding Allowed NO
Water Quality NO

Infiltration Method HORTON

Flow Routing Method DYNWAVE

Surcharge Method EXTRAN

Starting Date 04/11/2022 00:00:00

Ending Date 04/12/2022 12:00:00

Antecedent Dry Days 0.0

Report Time Step 00:01:00

Wet Time Step 00:05:00

Dry Time Step 00:05:00

Routing Time Step 2.00 sec

Variable Time Step YES

Maximum Trials 8

Number of Threads 1

Head Tolerance 0.001500 m

	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm

Total Precipitation	0.495	149.985
Evaporation Loss	0.000	0.000
Infiltration Loss	0.011	3.380
Surface Runoff	0.478	144.918
Final Storage	0.007	2.003
Continuity Error (%)	-0.211	

	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr

Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.478	4.779
Groundwater Inflow	0.000	0.000

```

RDII Inflow ..... 0.000 0.000
External Inflow ..... 0.000 0.000
External Outflow ..... 0.457 4.573
Flooding Loss ..... 0.000 0.000
Evaporation Loss ..... 0.000 0.000
Exfiltration Loss ..... 0.000 0.000
Initial Stored Volume .... 0.000 0.000
Final Stored Volume ..... 0.019 0.195
Continuity Error (%) ..... 0.232

```

```

*****
Time-Step Critical Elements
*****
None

```

```

*****
Highest Flow Instability Indexes
*****
Link C1_1 (54)

```

```

*****
Routing Time Step Summary
*****
Minimum Time Step      : 1.50 sec
Average Time Step      : 2.00 sec
Maximum Time Step      : 2.00 sec
Percent in Steady State : 0.00
Average Iterations per Step : 2.00
Percent Not Converging  : 0.01
Time Step Frequencies :
  2.000 - 1.516 sec    : 100.00 %
  1.516 - 1.149 sec    : 0.00 %
  1.149 - 0.871 sec    : 0.00 %
  0.871 - 0.660 sec    : 0.00 %
  0.660 - 0.500 sec    : 0.00 %

```

```

*****
Subcatchment Runoff Summary
*****

```

Subcatchment	Total Precip mm	Total Runon mm	Total Evap mm	Total Infil mm	Imperv Runoff mm	Perv Runoff mm	Total Runoff mm	Total Runoff 10 ⁶ ltr	Peak Runoff CMS	Runoff Coeff
S1	149.98	0.00	0.00	3.38	133.55	11.37	144.92	4.78	1.21	0.966

```

*****
Node Depth Summary
*****

```


Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
J1	JUNCTION	0.27	0.95	175.02	0 09:08	0.84
6R3879	OUTFALL	0.27	0.46	174.51	1 00:20	0.46
SU1	STORAGE	0.28	1.60	175.70	0 09:32	1.60

Node Inflow Summary

Node	Type	Maximum Lateral Inflow CMS	Maximum Total Inflow CMS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 ltr	Total Inflow Volume 10^6 ltr	Flow Balance Error Percent
J1	JUNCTION	0.000	0.449	0 09:32	0	4.57	-0.102
6R3879	OUTFALL	0.000	0.449	0 09:32	0	4.57	0.000
SU1	STORAGE	1.211	1.211	0 09:15	4.78	4.78	0.369

Node Surcharge Summary

Surcharging occurs when water rises above the top of the highest conduit.

Node	Type	Hours Surcharged	Max. Height Above Crown Meters	Min. Depth Below Rim Meters
J1	JUNCTION	1.11	0.427	0.788

Node Flooding Summary

No nodes were flooded.

Storage Volume Summary

Storage Unit	Average Volume 1000 m3	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m3	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow CMS
SU1	0.216	12	0	0	1.082	60	0 09:32	0.449

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CMS	Max Flow CMS	Total Volume 10^6 ltr
6R3879	63.06	0.056	0.449	4.573
System	63.06	0.056	0.449	4.573

 Link Flow Summary

Link	Type	Maximum Flow CMS	Time of Max Occurrence days hr:min	Maximum Veloc m/sec	Max/ Full Flow	Max/ Full Depth
C1_2	CONDUIT	0.449	0 09:32	2.15	2.86	0.93
C1_1	ORIFICE	0.449	0 09:32			1.00

 Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class									
		Up Dry	Down Dry	Sub Dry	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl		
C1_2	1.00	0.00	0.00	0.00	1.00	0.00	0.00	0.00	0.00	0.00	0.00

 Conduit Surcharge Summary

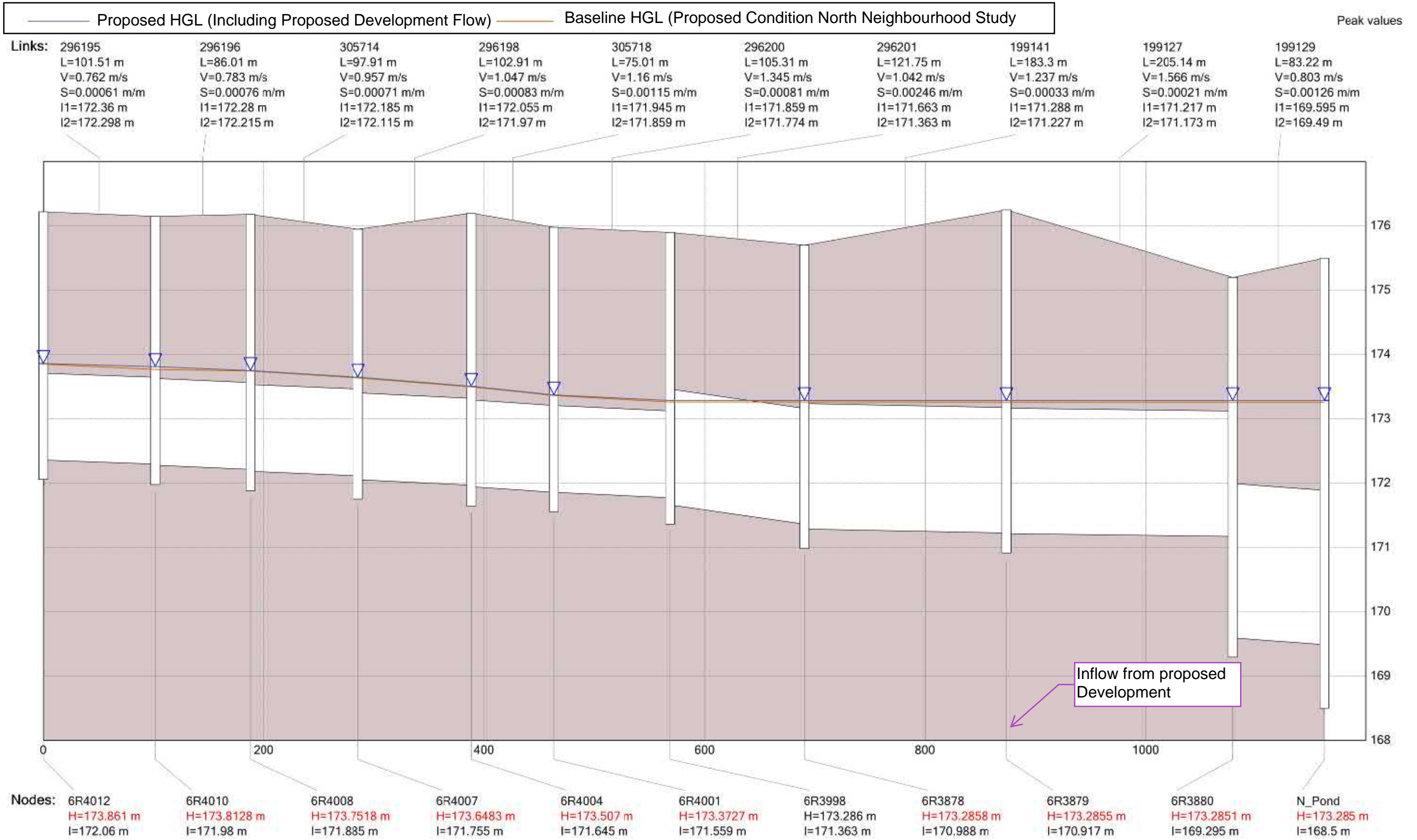
Conduit	Hours Full			Hours Above Normal	Hours Full Capacity Limited
	Both Ends	Upstream	Dnstream	Flow	
C1_2	0.01	1.11	0.01	1.66	0.01

Analysis begun on: Thu Jun 30 09:28:59 2022
 Analysis ended on: Thu Jun 30 09:29:00 2022
 Total elapsed time: 00:00:01

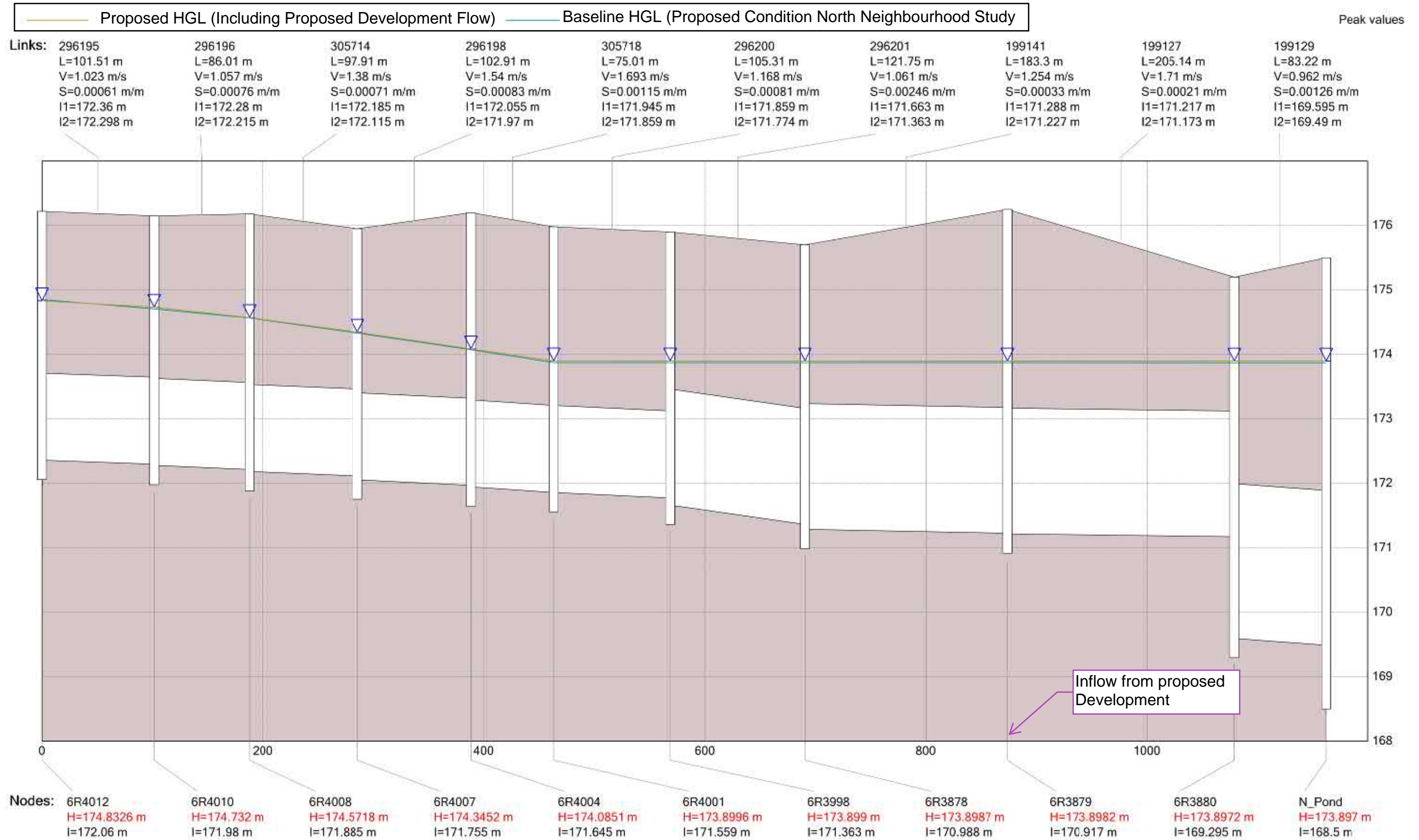
Appendix C

Wyandotte Street East Sewer Profile Comparison

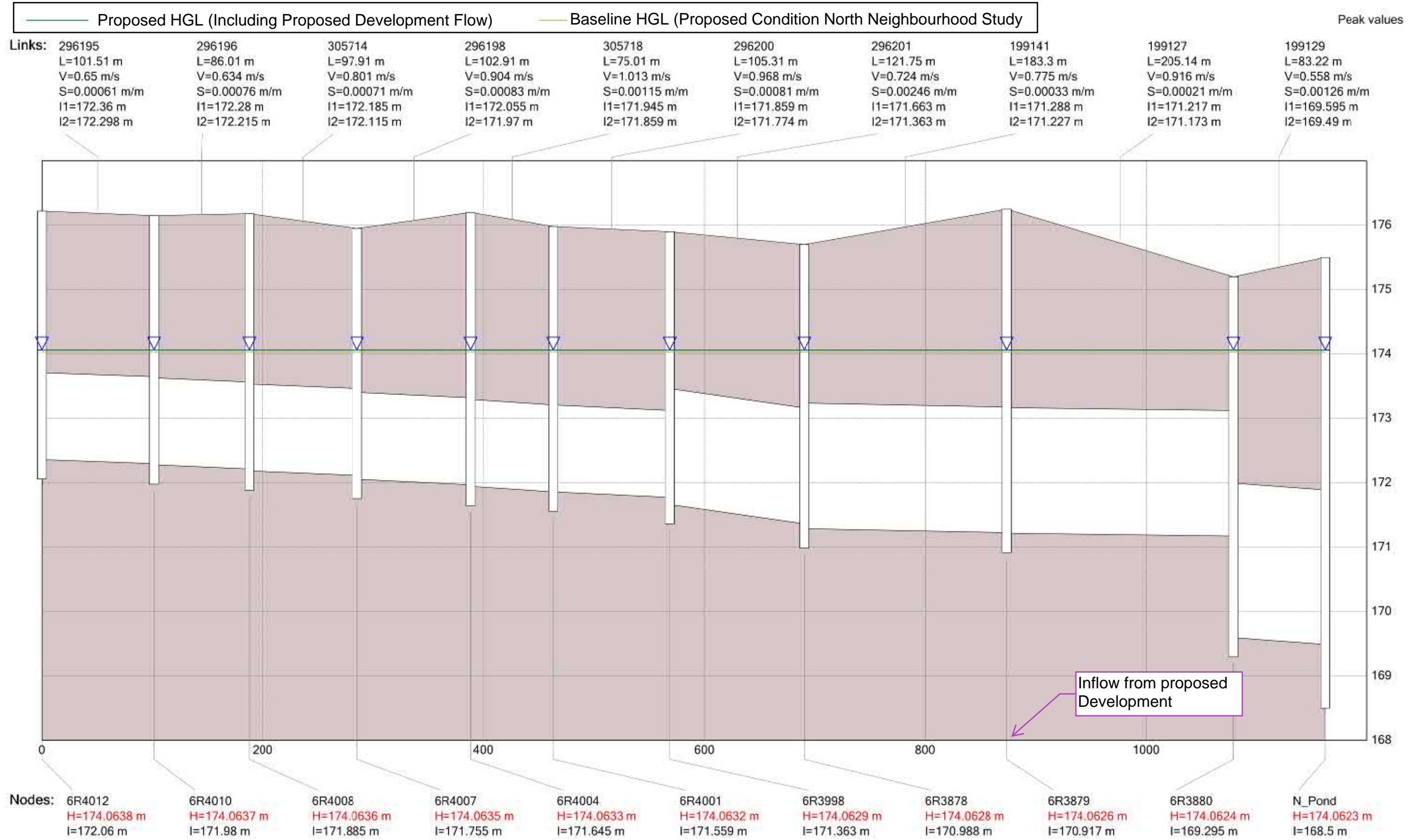
Wyandotte Sewer HGL Profile Comparison (1:5 year 4 hour)



Wyandotte Sewer HGL Profile Comparison (1:100 year 4 hour)



Wyandotte Sewer HGL Profile Comparison (1:100 year 24 hour)



Appendix D

Details of the OGS Unit

ADS OGS Sizing Summary

Project Name:	Ganatchio Gardens	
Consulting Engineer:	Dillon	
Location:	Windsor, ON	
Sizing Completed By:	C. Neath	Email: cody.neath@ads-pipe.com

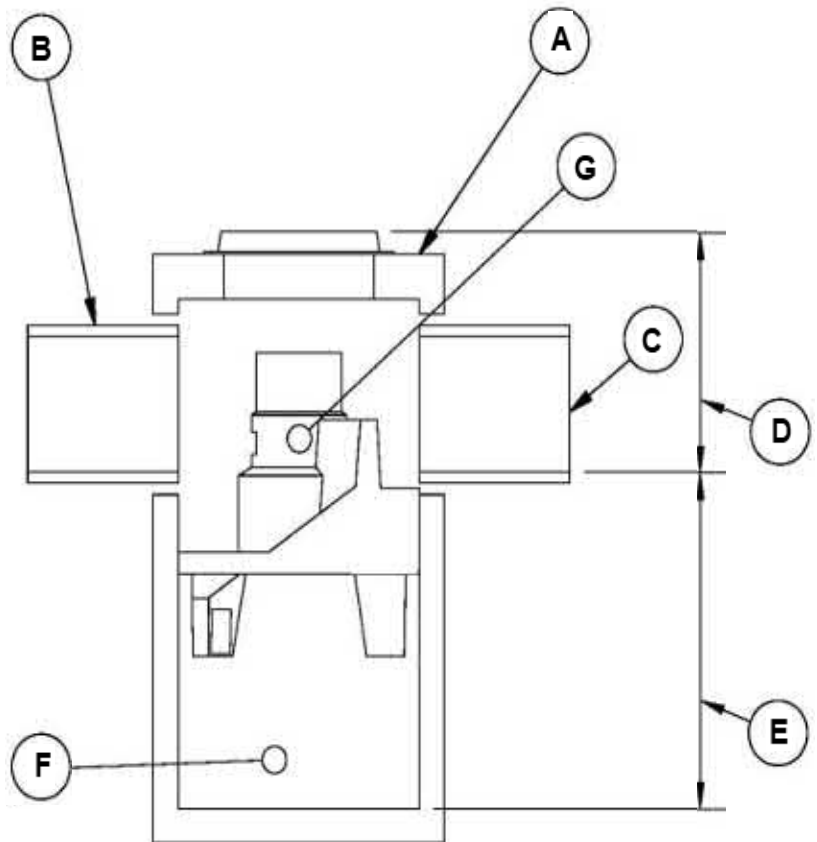
Treatment Requirements		
Treatment Goal:	Normal (MOE)	
Selected Parameters:	70% TSS	90% Volume
Selected Unit:	FD-5HC	

Site Details	
Site Area:	3.3 ha
% Impervious:	90%
Rational C:	0.84
Rainfall Station:	Windsor, ONT
Particle Size Distribution:	Fine
Peak Flowrate:	417 L/s

Summary of Results		
Model	TSS Removal	Volume Treated
FD-4HC	69.0%	78.2%
FD-5HC	72.0%	>90%
FD-6HC	74.0%	>90%
FD-8HC	79.0%	>90%
FD-10HC	82.0%	>90%

FD-5HC Specification	
Unit Diameter (A):	1,500 mm
Inlet Pipe Diameter (B):	300 mm
Outlet Pipe Diameter (C):	300 mm
Height, T/G to Outlet Invert (D):	2000 mm
Height, Outlet Invert to Sump (E):	1780 mm
Sediment Storage Capacity (F):	1.29 m ³
Oil Storage Capacity (G):	1,135 L
Recommended Sediment Depth for Maintenance:	475 mm
Max. Pipe Diameter:	600 mm
Peak Flow Capacity:	566 L/s

Site Elevations:	
Rim Elevation:	100.00
Inlet Pipe Elevation:	98.00
Outlet Pipe Elevation:	98.00



Notes:

Removal efficiencies are based on NJDEP Test Protocols and independently verified.

All units supplied by ADS have numerous local, provincial, and international certifications (copies of which can be provided upon request). The design engineer is responsible for ensuring compliance with applicable regulations.



Project Name: Ganatchio Gardens
 Consulting Engineer: Dillon
 Location: Windsor, ON

Net Annual Removal Efficiency Summary: FD-5HC

Rainfall Intensity ⁽¹⁾	Rational Equation Flowrate	Surface Loading Rate	Fraction of Rainfall ⁽¹⁾	FD-5HC Removal Efficiency	Weighted Net-Annual Removal Efficiency
mm/hr	L/s	L/min/m ²	%	%	%
3.00	23.1	784	13.2%	81%	10.7%
4.00	30.8	1046	9.6%	79%	7.6%
5.00	38.5	1307	7.5%	78%	5.8%
6.00	46.2	1569	6.0%	76%	4.6%
7.00	53.9	1830	4.8%	75%	3.6%
8.00	61.6	2092	4.1%	74%	3.0%
9.00	69.3	2353	3.6%	73%	2.6%
10.00	77.0	2614	3.2%	73%	2.3%
11.00	84.7	2876	2.8%	72%	2.0%
12.00	92.4	3137	2.5%	71%	1.8%
15.00	115.5	3922	6.6%	70%	4.6%
20.00	154.0	5229	8.3%	68%	5.7%
25.00	192.5	6536	5.8%	67%	3.9%
30.00	231.0	7843	4.6%	66%	3.0%
35.00	269.5	9150	3.8%	65%	2.5%
40.00	308.0	10458	2.9%	64%	1.9%
45.00	346.5	11765	2.4%	63%	1.5%
50.00	385.0	13072	1.8%	63%	1.1%
65.00	500.5	16994	6.6%	61%	4.0%
Total Net Annual Removal Efficiency:					72.0%
Total Runoff Volume Treated:					99.9%

Notes:

- (1) Based on Windsor/Essex Region Stormwater Manual 2018, Table 3.4.1.5
- (2) Based on third party verified data and approximating the removal of a PSD similar to the STC Fine distribution